

42, 43 and 45 30CPS Character Printers

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REPAIR MANUAL 523 Issue 2, February 1984

POWER SUPPLIES USED WITH 42, 43 AND 45-30 CPS CHARACTER PRINTERS

REPAIR MANUAL

INTRODUCTION

This manual provides complete repair information for power supplies used with 42, 43 and 45-30 CPS Character Printers. The manual is intended for field or shop use and is arranged into various parts that include testing, troubleshooting, circuit descriptions and diagrams, parts and packing and marking.

Waveforms are included on circuit diagrams and charts are provided for additional trouble isolation using an oscilloscope or volt-ohmmeter.

Circuit Diagram Manual 385 provides circuit information extracted from this manual. The component layouts, lead designations and circuit diagrams for each circuit are combined into single foldout sheets for the convenience of field or shop personnel when repairing circuit cards.

The task flow chart on the next page illustrates the intended repair activities and the associated manual parts.

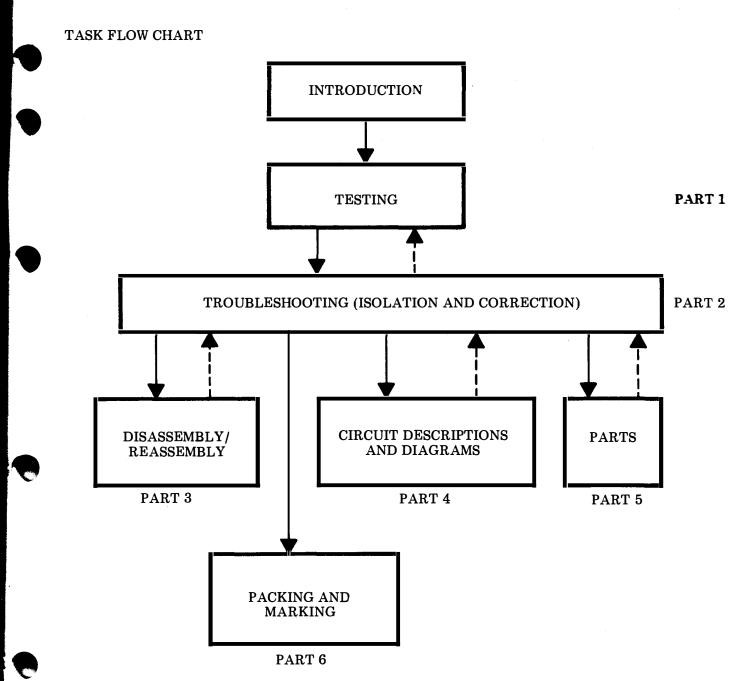
Spare parts for repair are available from Teletype Corporation. Service personnel should be properly trained and have access to these spares before attempting repair of circuit cards.

This manual is intended to be used with the following supplemental repair documentation for the 42/43and 45-30 CPS Character Printers.

MANUAL NO.

DESCRIPTION

- 385 - Circuit Diagrams for Components used in 42/43 and 45-30 CPS Character Printer Terminals and Associated Units - Product Support Manual 416 - 42/43 Paper Tape Unit 442 - TTL and SSI Logic Cards used in 42/43 and 45-30 CPS Character Printers 522
- Keyboards used in 42/43 Basic Terminals 525
- SSI Keyboards used in 42/43 Buffered Terminals 530
- 533 - Parts - Enclosures, Paper Handling and Miscellaneous Accessories used with 42/43 and 45-30 CPS Character Printers
- 534 - Interfaces, Controllers and Modification Kit Circuit Cards associated with 42/43 Terminals (includes AB, SCU and brief repair of non-pedestal controllers)
- -42/43 and 45-30 CPS Character Printer Mechanisms 539
- 568 - Internal Modems used in 42 Basic Terminals



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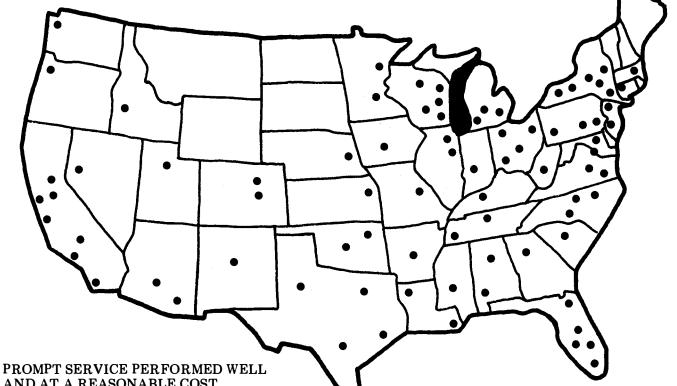
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REPAIR MANUAL FOR POWER SUPPLIES USED WITH 42, 43 and 45-30 CPS CHARACTER PRINTERS

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PART 1	TESTING
PART 2	TROUBLESHOOTING
PART 3	DISASSEMBLY/REASSEMBLY
PART 4	CIRCUIT DESCRIPTIONS AND DIAGRAMS
PART 5	PARTS
PART 6	PACKING AND MARKING

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PART 1 – TESTING

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A. GENERAL

This part provides testing requirements and procedures for the power supplies used with 42, 43 and 45-30 CPS Character Printers. The 430700, 430760, 430770 and 430780 power supply assemblies are included in this part.

Note: When ordering replaceable parts or components, unless otherwise specified, prefix each part number with the letters "TP" (ie, TP410055).

The information in this part is intended to determine if the power supply is operating properly and will continue to operate for extended periods under normal operating conditions.

Endurance, environmental extreme or electrical parameter testing information is not provided in this part.

The testing information provided herein should normally be used to determine if:

- (1) A repaired power supply is operating properly before being returned to a customer or placed in service.
- (2) A questionable power supply is operating properly or requires repair.

Warning: Repair or troubleshooting of these power supplies should not be attempted unless a power isolation transformer is connected between the ac input power and the supply.

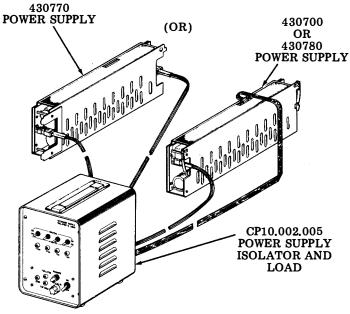
Following any repairs of the 430700 and 430780 power supply assemblies the following high voltage breakdown test must be performed:

With Pins 1 and 3 tied together at input connector (J202), a 1500 Vac (RMS) potential between these pins and Pin 2 (G) shall be applied with 30 second rise, 60 second hold time with no evidence of breakdown, and the peak current shall not exceed 10 mA. This requirement may be met at the set level.

B. TEST EQUIPMENT

The 430700, 430770 and 430780 power supplies may be tested as a loose component using the CP10.002.005 power supply isolator and load which provides an isolated nominal 117 Vac input voltage and resistive loads for power supply output voltages. Refer to Users Guide Manual 419 for theory of operation.

Contact Teletype Corporation, Custom Systems Division, 312-982-2000 for test equipment ordering information.



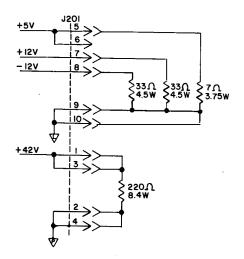
C. TESTING PROCEDURES

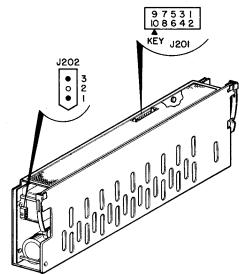
Loose power supplies may be tested as part of a teleprinter terminal. If a loose power supply is installed into a teleprinter terminal and the teleprinter passes the appropriate service manual tests and the test on Page 1-1 (430700 and 430780), the power supply may be considered good.

Power supplies may be tested as loose components using the following test procedures. The test on Page 1-1 must also be performed (430700 and 430780).

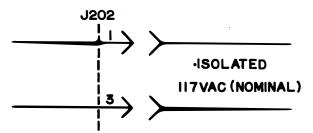
430700 and 430780 Power Supply

Connect load resistors to the J201 connector as shown below:





Connect any isolated voltage between 103 and 127 Vac and between 48 and 62 Hz to the J202 connector as follows:



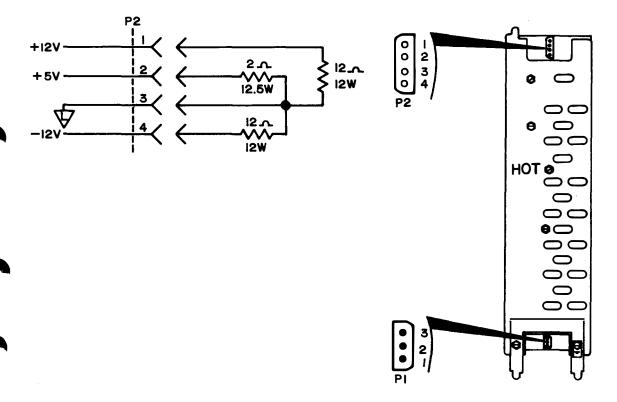
Verify the voltages shown below are present at the J201 connector and meet the voltage limits and maximum ripple requirements.

Nominal Voltage	Voltage Limits	Maximum Ripple (Peak to Peak)	J201 Connector No.
Logic Ground -12 Vdc +12 Vdc +5 Vdc Power Ground +42 Vdc	-11.0 V to -13.0 V 11.0 V to 13.0 V 4.6 V to 5.4 V 38.6 V to 45.4 V	100 MV 100 MV 50 MV 500 MV	9 and 10 8 7 5 and 6 2 and 4 1 and 3

Verify LED (Light Emitting Diode) is ON.

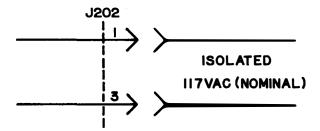
430770 Power Supply

Connect load resistors to the P2 connector as shown below:



C. TESTING PROCEDURES

Connect any isolated voltage between 103 and 127 Vac and between 48 and 62 Hz to the P1 connector as follows:



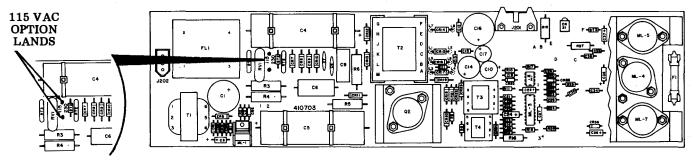
Verify the voltages shown below are present at the P2 connector and meet the voltage limits and maximum ripple requirements.

Nominal Voltage	Voltage Limits (Including Ripple)	Maximum Ripple (Peak to Peak)	J201 Connector No.
Logic Ground +5 Vdc +12 Vdc -12 Vdc	4.75 V to 5.25 V 11.40 V to 12.60 V -11.40 V to -12.50 V	200 MV 240 MV 240 MV	3 2 1 4

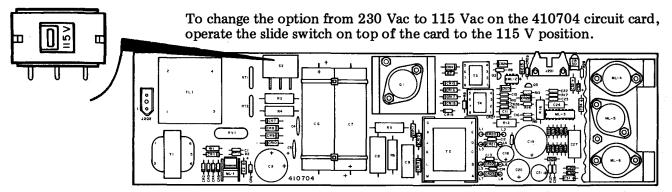
430760 Power Supply

The 430760 power supply may be optioned for 230 Vac or 117 Vac operation. Note the position of strap ST2 on the 410703 circuit card.

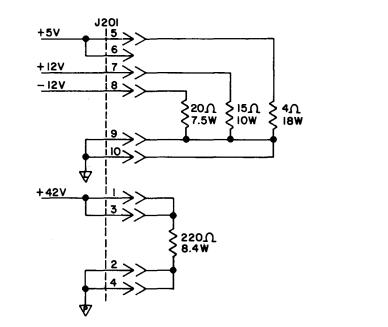
The 410703 circuit card is shown optioned for 230 Vac. To option the 410703 circuit card for 115 Vac, remove strap ST2 from its 230 Vac location and solder it into the 115 Vac position.

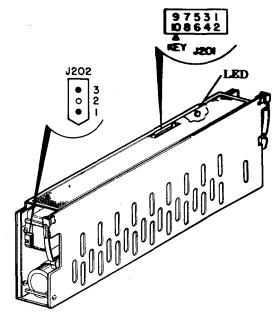


410703 CIRCUIT CARD



410704 CIRCUIT CARD



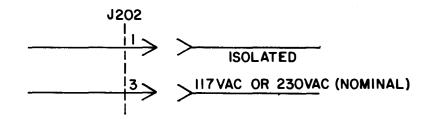


Connect load resistors to the J201 connector as shown below:

If ST2 is in the 230 position, connect any isolated voltage between 196 Vac and 264 Vac and between 48 and 62 Hz to the J202 connector.

If ST2 is in the 115 position connect any isolated voltage between 103 Vac and 127 Vac and between 48 and 62 Hz to the J202 connector.

Connect the proper voltage to the J202 connector as follows:



Verify the voltages shown below are present at the J201 connector and meet the voltage limits and maximum ripple requirements.

Nominal Voltage	Voltage Limits	Maximum Ripple (Peak to Peak)	J201 Connector No.
Logic Ground -12 Vdc +12 Vdc +5 Vdc Power Ground +42 Vdc	-11.28 V to 12.72 V 11.28 V to 12.72 V 4.75 V to 5.25 V 38.6 V to 42.0 V	250 MV 250 MV 250 MV 850 MV	9 and 10 8 7 5 and 6 2 and 4 1 and 3

Verify LED (Light Emitting Diode) is ON.

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A. GENERAL

This part provides troubleshooting information for power supplies used with 42, 43 and 45-30 CPS Character Printers. The 430700, 430760, 430770 and 430780 power supply assemblies are included in this part. No Troubleshooting Guide for the 430770 power supply is provided in this part.

Note: When ordering replaceable parts or components, unless otherwise specified, prefix each part number with the letters "TP" (ie, TP410055).

Check and verify proper static circuit resistance of defective power supply assemblies before connecting them to the teleprinter or power source, to prevent overloading and blowing the fuse when power is turned on.

When replacing the power supply fuse, wait 10 seconds after turning off power before removing fuse.

Use meter RX1 scale when making resistance readings. Resistance readings shown are approximate and may be higher or lower than those specified, depending on the meter used.

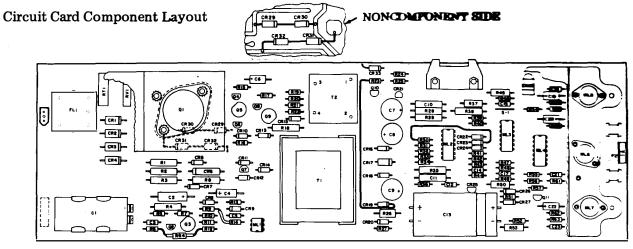
Before applying power to 430700 power supply assemblies with cover or heat sink removed, or attempting repair of the power supply, refer to Part 3 - DISASSEMBLY/REASSEMBLY, and check for vented capacitors.

The voltage regulator circuitry, oscillator circuitry, and pulse width modulator circuitry of the 430700, 430760 and 430780 power supply assemblies may be checked by applying external dc voltages with no ac power applied. (Refer to the respective circuit diagram for specific voltages and points of application.)

B. 430700 AND 430780 POWER SUPPLY

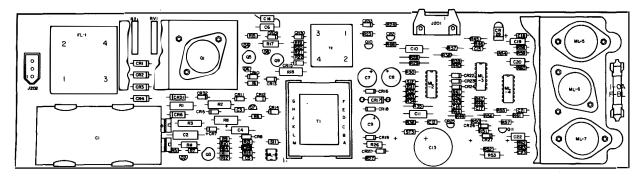
Troubleshooting Guide

]	QUESTION	YES	NO
1.	Is the red indicator ON (power applied and on)?	Go to 1c.	Go to 1a.
1a.	Is +16 V present at the anode of CR28?	Replace CR28.	Go to 1b.
1b.	Are any voltages present on J201? Pins 5, 6 +5 V Pin 8 -12 V Pin 7 +12 V Pins 1, 3 +42 V	Go to 1c.	Check oscillator and con- trol circuit (see Note 202 on circuit diagram in Part 4). Check components in ac-dc circuit. Check components in over- voltage circuit if present. Check components in primary circuit
1c.	Is +5 V present and within range on J201 Pin 5?	Go to 1d.	Check CR16. Check ML5. Check ML3. Check T1 (F-M).
1d.	Is -12 V present and within range of J201 Pin 8?	Go to 1e.	Check CR18. Check ML6. Check ML3. Check T1 (C-D).
1e.	Is +12 V present and within range on J201 Pin 7?	Go to 1f.	Check CR19. Check ML7. Check ML3. Check T1 (B-C).
1f.	Is +42 V present and within range on J201 Pins 1 and 3?	Go to 2.	Check fuse F2. Check CR17. Check ML3. Check T1 (E-A).
2.	Are all voltages present and within range on J201?	If LED is OFF check ML4. If LED is ON go to 3.	Review initial indication of trouble.
3.	Did the power supply meet the requirements of the high voltage breakdown test on Page 1-1?	Undefined problem. Refer to Circuit Des- criptions and Circuit Diagrams.	Check FL1. Check C16. Check for arc under Q1. Check for arc through plastic tubing on C1 to the capacitor clamp. Check ML1. Check T2. Check T1.

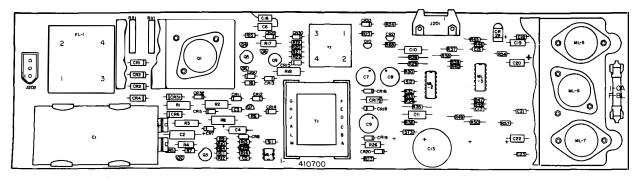


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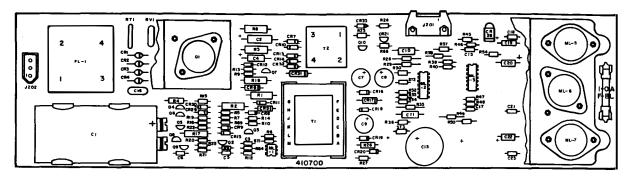
410700 Circuit Card Issues 1 through 4



410700 Circuit Card Issues 5 through 8B

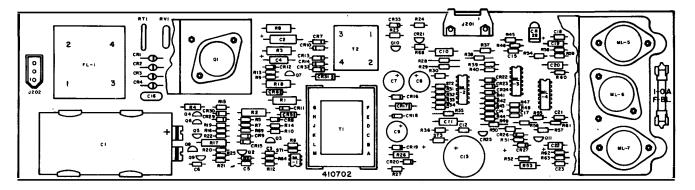


410700 Circuit Card Issue 9

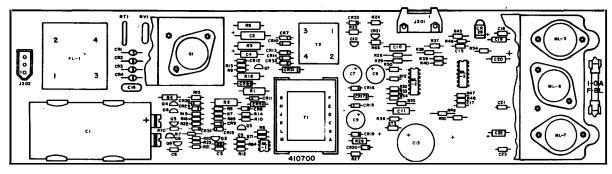


410700 Circuit Card Issue 10

B. 430700 and 430780 POWER SUPPLY (Contd)



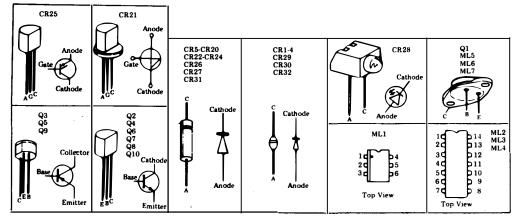
410702 Circuit Card Issues 1A through 2B



410702 Circuit Card Issue 3

Some parts shown are not present on later issue circuit cards (refer to PART 5-PARTS).

Semiconductors and Integrated Circuits Identification and Lead Designation.



COMPONEN	T RESISTAL	NCE (Approx)	COMPO	NENT	<u>RESISTA</u>	NCE (Approx)
CR1	28	ohms	Q1	B-E	2/	l ohms
CR2		ohms	4-	B-C		2 ohms
CR3		ohms	Q2	B-E) oh ms
CR4		ohms	4-	B-C) ohms
CR5		ohms	Q3	B-E		2 ohms
CR6		ohms	40	B-C		2 ohms
CR7		ohms	Q4	B-E) ohms
CR8		ohms	v € +	B-C) ohms
CR9		ohms	Q5	B-E) ohms
CR10		ohms	40	B-C) ohms
CR11		ohms	Q6	B-E) ohms
CR12		ohms	Q U	B-E B-C) ohms
CR12		ohms	Q7	B-E) ohms
CR13 CR14		ohms	QI	B-E B-C) ohms
CR14 CR15		ohms	Q8	B-C B-E) ohms
CR15 CR16		ohms	୍ବତ	B-E B-C) ohms
		ohms	00			
CR17		ohms	Q9	B-E) ohms
CR18		ohms	010	B-C) ohms
CR19		ohms	Q10	B-E) ohms
CR20		ohms	011	B-C) ohms
		ohms	Q11	B-E) ohms
CR22	G-A 42	ohms		B-C	30) ohms
		ohms	N/T 1	1 0		、 ,
CR23		ohms	ML1) ohms
CR24		ohms		4-6		3 ohms
		ohms		5-6	48	3 ohms
		ohms	MTE	DE		` 1
CR26		ohms	ML5) ohms
CR27 CR28		ohms (LED on)		B-C	25	5 ohms
CR29		ohms	ML6	DF	70) ohms
CR25 CR30		ohms	MLO	B-E B-C		5 ohms
CR31		ohms		D- C	21) 011115
CR32		ohms	ML7	DF	20	3 ohms
CR33		ohms		B-E B-C		5 ohms
				р-С	24	Johns
Static Circui	t Resistance (See	Note)				
<u>CONNECTO</u>	OR TERMINAL	REFEREN	CE POINT	• 2	RESISTAN	CE (Approx)
	- /				LO	HI
	6 (+5 V)		9 (logic gnd		38 ohms	2K ohms
	7 (+12 V)		9 (logic gnd		32 ohms	400 ohms
	8 (-12 V)		9 (logic gnd		70 ohms	8K ohms
J201 —	1 (+42 V)	J201 - 2	2 (power gn	ld)	24 ohms	5K ohms

 ${\bf Semiconductor-In\ Circuit\ Static\ Forward\ Resistance}$

Note: Take resistance reading, reverse meter leads and take second resistance reading.

C. 430760 POWER SUPPLY

410703 Circuit Card Troubleshooting Guide

QUESTION		YES	NO
1.	Is the red indicator ON (power applied and on)?	Go to 1b.	Go to 1a.
1a.	Is +42 V present and within range on J201 Pins 1 and 3?	Replace CR31.	Check fuse F1. Go to 1b.
1b.	Are any voltages present on J201?	Go to 2.	Go to 1c.
	Pins 5, 6 +5 V Pin 8 -12 V Pin 7 +12 V Pins 1, 3 +42 V		
1c.	Is voltage present and correct across V+ and VIN?	Go to 1d.	Check filter FL1. Check VIN Bridge Rectifier.
1d.	Is V Start voltage present and correct?	Check ML2 and ML3 Check components in primary circuit.	Check ML1, CR6. Check V Start Bridge Rec- tifier.
2.	Is +42 V present and within range on J201 Pins 1 and 3?	Go to 2a.	Check fuse F1, CR14, ML3. Check T1 (E-F).
2a.	Is +5 V present and within range on J201 Pins 5 and 6?	Go to 2b.	Check CR17, ML5, ML3. Check T1 (A-C).
2b.	Is +12 V present and within range on J201 Pin 7?	Go to 2c.	Check CR16, ML7, ML3. Check T1 (B-C).
2c.	Is -12 V present and within range on J201 Pin 8?	Go to 3.	Check CR15, ML6, ML3. Check T1 (C-D).
3.	Are all voltages present and correct on J201?	Undefined Problem- Refer to Circuit Descriptions and Circuit Diagrams.	Review initial indication of trouble.

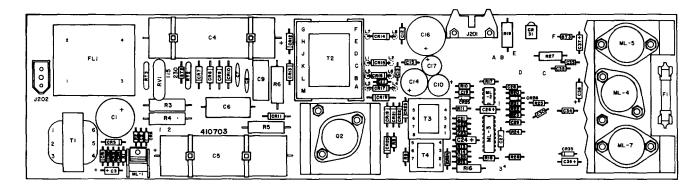
MANUAL 523, 2-7

410704 Circuit Card Troubleshooting Guide

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	QUESTION	YES	NO
1.	Is the red indicator ON (power applied and on)?	Go to 1b.	Go to 1a.
1a.	Is +5 V present and within range on J201 Pins 5 and 6?	Replace CR30.	Go to 1b.
1b.	Are any voltages present on J201?	Go to 2.	Go to 1c.
	Pins 5, 6 +5 V Pin 8 -12 V Pin 7 +12 V Pins 1, 3 +42 V		
1c.	Is voltage present and correct across V+ and VIN?	Go to 1d.	Check filter FL1. Check VIN Bridge Rectifier.
1d.	Is V Start voltage present and correct?	Check ML2, ML3, Q2, and Q3. Check compo- nents in primary circuit.	Check ML1, CR6. Check V Start Bridge Rec- tifier.
2.	Is +42 V present and within range on J201 Pins 1 and 3?	Go to 2a.	Check CR22 and ML3. Check T1 (E-F).
2a.	Is +5 V present and within range on J201 Pins 5 and 6?	Go to 2b.	Check CR23, ML6, ML3. Check T1 (A-C).
2b.	Is +12 V present and within range on J201 Pin 7?	Go to 2c.	Check CR22, ML4, ML3. Check T1 (B-C).
2c.	Is -12 V present and within range on J201 Pin 8?	Go to 3.	Check CR21, ML5, ML3. Check T1 (C-D).
3.	Are all voltages present and correct on J201?	Undefined Problem- Refer to Circuit Descriptions and Circuit Diagrams.	Review initial indication of trouble.

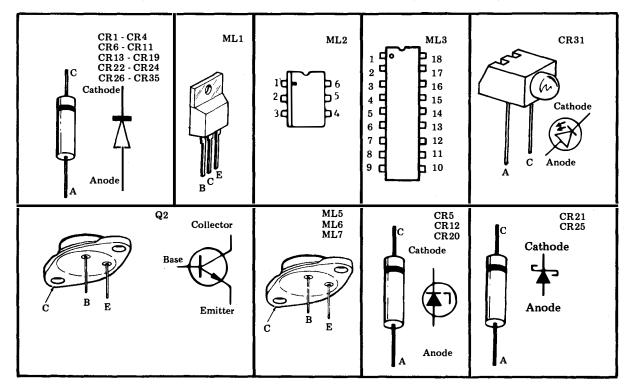
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410703 Circuit Card Component Layout

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Semiconductors and Integrated Circuits Identification and Lead Designation



1

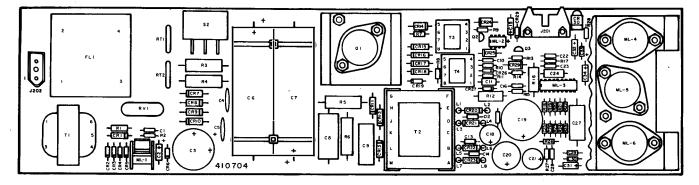
COMPONENT	RESISTANCE (A	pprox) COMPON	ENT	RESISTA	NCE (Approx)
CR1	28 ohms	CR18		28	ohms
CR2	28 ohms	CR19			ohms
CR3	28 ohms	CR20)		oh ms
CR4	28 ohms	CR21			ohms
CR5	30 ohms	CR22			ohms
CR6	28 ohms	*CR23		28	ohms
CR7	26 ohms	CR24	:	10	ohms
CR8	26 ohms	CR25		10	ohms
CR9	26 ohms	CR26	5	28	ohms
CR10	26 ohms	CR35	•	28	ohms
CR11	24 ohms	Q2	B-E	8	ohms
CR12	24 ohms		B-C	22	ohms
CR13	24 ohms		E-C	28	ohms
CR14	22 ohms	ML1	B-E	36	ohms
CR15	22 ohms		B-C	30	ohms
CR16	22 ohms				
CR17	22 ohms	ML5	B-E	22	ohms
			B-C	34	ohms
		ML6	B-E	22	ohms
			B-C	110	ohms
		ML7	B-E	22	ohms
			B-C		ohms
Static Circuit Resistan	ce (See Note)				
CONNECTOR TE	RMINAL	REFERENCE POINT		RESISTANCE	E (Approx)
				LO	<u>HI</u>
J201 — 6 (+5	V)	J201 — 9 (logic gnd)		28 ohms	500 ohms
J201 - 7 (+1)		J201 - 9 (logic gird)		40 ohms	
J201 - 8 (-12)		J201 - 9 (logic gnd)		115 ohms	
J201 - 1(+4)		J201 - 2 (power gnd)		22 ohms	
	- · /			011115	

Semiconductor - In Circuit Static Forward Resistance

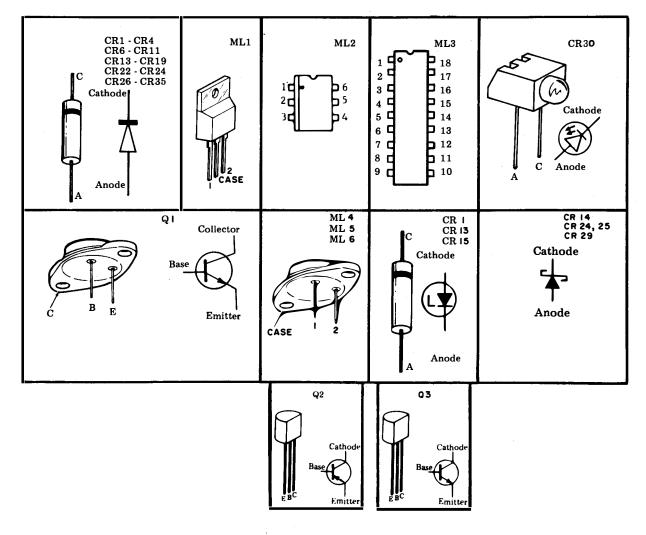
Note: Take resistance reading, reverse meter leads and take second resistance reading.



410704 Circuit Card Component Layout



SEMICONDUCTORS AND INTEGRATED CIRCUITS IDENTIFICATION AND LEAD DESIGNATION



523, 2-10

COMPONENT	RESISTANCE (Approx)	COMPONENT	RESISTANCE (Approx)
CR1	30 ohms	CR23	22 ohms
CR2	28 ohms	CR24	10 ohms
CR3	28 ohms	CR25	10 ohms
CR4	28 ohms	CR26	28 ohms
CR5	28 ohms	CR27	10 ohms
CR6	28 ohms	CR28	28 ohms
CR7	26 ohms	Q1 B-E	8 ohms
CR8	26 ohms	B-C	28 ohms
CR9	26 ohms	Q2 B-E	30 ohms
CR10	26 ohms	B-C	30 ohms
CR11	24 ohms	Е-С	40 ohms
CR12	24 ohms	Q3 B-E	30 ohms
CR13	24 ohms	B-C	30 ohms
CR14	8 ohms	E-C	40 ohms
CR15	32 ohms	ML1 B-E	36 ohms
CR16	26 ohms	B-C	30 ohms
CR17	28 ohms	ML4 B-E	22 ohms
CR18	30 ohms	B-C	38 ohms
CR19	28 ohms	ML5 B-E	22 ohms
CR20	22 ohms	B-C	110 ohms
CR21	22 ohms	ML6 B-E	22 ohms
CR22	22 ohms	B-C	34 ohms

 ${\rm Semiconductor-In\ Circuit\ Static\ Forward\ Resistance}$

Static Circuit Resistance

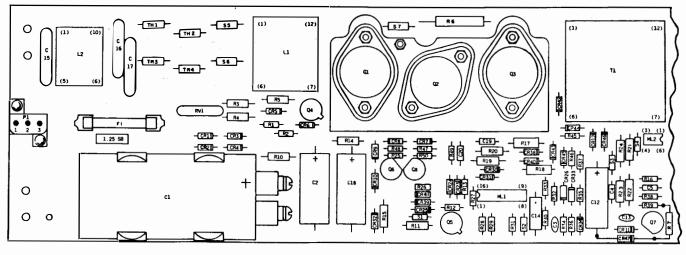
(See Note.)

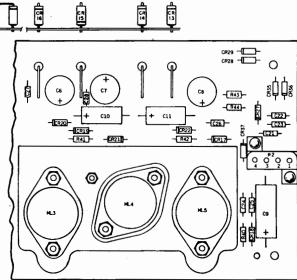
CONNECTOR TERMINAL	REFERENCE POINT	RESISTANCE (Approx)	
		<u>LO HI</u>	
J201 - 6 (+5 V) J201 - 7 (+12 V) J201 - 8 (-12 V) J201 - 1 (+42 V)	J201 — 9 (logic gnd) J201 — 9 (logic gnd) J201 — 9 (logic gnd) J201 — 9 (logic gnd) J201 — 2 (power gnd)	28 ohms 500 ohms 40 ohms 1 K ohms 115 ohms Infinity 22 ohms 750 ohms	

Note: Take resistance reading, reverse meter leads and take second resistance reading.

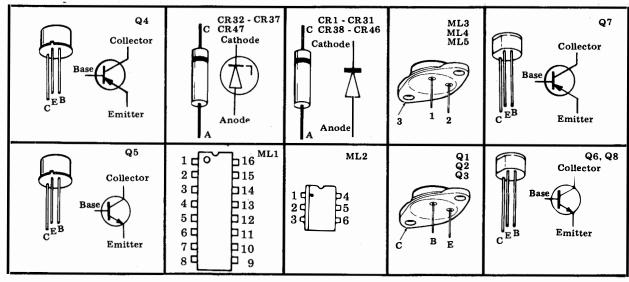
D. 430770 POWER SUPPLY

Circuit Card Component Layout





Semiconductors and Integrated Circuits Identification and Lead Designation



Semiconductor — In Circuit Static Forward Resistance

COMPONENT	RESISTANCE (Approx)	COMPONENT	RESISTANCE (Approx)
CR1	30 ohms	CR26	32 ohms
CR2	30 ohms	CR27	34 ohms
CR3	30 ohms	CR28	34 oh ms
CR4	30 ohms	CR29	34 ohms
CR5	24 ohms	CR30	34 ohms
CR6	26 ohms	CR31	34 ohms
CR7	24 ohms	CR32	34 ohms
CR8	24 ohms	CR33	34 ohms
CR9	30 ohms	CR34	33 ohms
CR10	30 ohms	CR35	32 ohms
CR11	35 ohms	CR36	35 ohms
CR12	30 ohms	CR37	35 ohms
CR13	22 ohms	CR38	28 ohms
CR14	22 ohms	CR39	25 ohms
CR15	24 ohms	CR40	34 ohms
CR16	24 ohms	CR41	34 ohms
CR17	32 ohms	CR42	32 ohms
CR18	30 ohms	CR43	32 ohms
CR19	30 ohms	CR44	32 ohms
CR20	28 ohms	CR45	32 ohms
CR21	28 ohms	CR46	32 ohms
CR22	32 ohms	CR47	32 ohms
CR23	34 ohms		
CR24	34 ohms		
CR25	34 ohms		

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D. 430770 POWER SUPPLY (Contd)

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COMP	ONENT	RESISTANCE (Approx)	COMPO	NENT	RESISTANCE (Approx)
Q1	B-E	25 ohms	ML2	1-2	60 ohms
Q1	B-C	25 ohms		4-6	48 ohms
Q2	B-E	28 ohms		5-6	40 ohms
Q2	B-C	28 ohms	ML3	3-1	24 ohms
Q3	B-E	28 ohms		3-2	32 ohms
Q3	B-C	28 ohms	ML4	1-3	24 ohms
Q4	B-E	35 ohms		1-2	32 ohms
Q 4	B-C	32 ohms	ML5	3-1	24 ohms
Q5	B-E	32 ohms		3-2	32 ohms
Q 5	B-C	32 ohms			
Q6	B-E	34 ohms			
Q6	B-C	34 ohms			
Q7	B-E	34 ohms			
Q7	B-C	34 ohms			
Q 8	B-E	34 ohms			
Q 8	B-C	34 ohms			

Static Circuit Resistance (See Note)

CONNECTOR TERMINAL	REFERENCE POINT	RESISTANCE (Approx)	
		LO <u>HI</u>	
P1-2 (+5 V)	P1-3 (logic gnd)	30 ohms 400 ohms	
P1-1 (+12 V)	P1-3 (logic gnd)	32 ohms 1.5K ohms	
P1-4 (-12 V)	P1-3 (logic gnd)	32 ohms 1.5K ohms	

Note: Take resistance reading, reverse meter leads and take second resistance reading.

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PART 3 - DISASSEMBLY/REASSEMBLY

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A. GENERAL

This part provides disassembly /reassembly procedures for power supplies used with 42, 43 and 45-30 CPS Character Printers. The 430700, 430760, 430770 and 430780 power supply assemblies are included in this part. When disassembly/reassembly information is not shown, the illustrations in PART 5 – PARTS provide sufficient information.

Note: When ordering replaceable parts or components, unless otherwise specified, prefix each part number with the letters "TP" (ie, TP410055).

Caution: Remove all power from the power supply before performing any disassembly/reassembly procedures.

When removing a part, do not pry or force parts to provide the necessary clearance for removal. Follow the removal procedure and note how each part is removed and the sequence of its removal so that proper reassembly can be accomplished. For reassembly, reverse the removal procedures except where different instructions are given.

B. TOOLS REQUIRED

The following tools may be required when performing the power supply disassembly/reassembly procedures. Most of these items should normally be present in standard maintenance tool kits.

<u>Part No.</u>	Description
75765	Hook, Pull Spring
94646	Stick, Orange
95368	Screwdriver, 1/8 Inch, 2 Inch Blade
100982	Screwdriver/Clip, 1/4 Inch, 6 Inch Blade
108285	Pliers, Long-Nose
151392	Tweezers
348097	Driver, Nut, 1/4 Inch
348098	Driver, Nut, 5/16 Inch
407326	Extractor, IC
408071	Pliers, Cutting

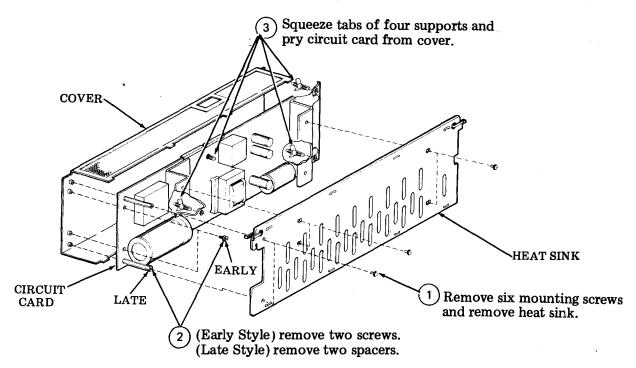
Customer Provided Tools

Soldering Iron (Low Wattage, Grounded) Desoldering Tool

C. DISASSEMBLY/REASSEMBLY

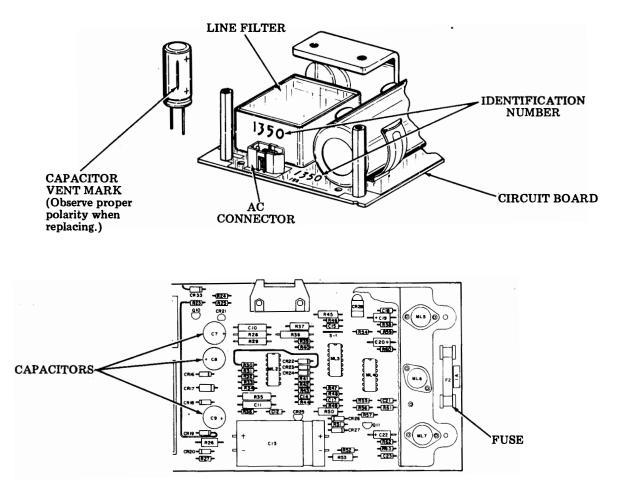
1. <u>430700 and 430780 Power Supply</u>

(a) 410700 and 410702 Circuit Card Removal



(b) Vented Capacitors (410700 Circuit Card, Issue 4D or earlier).

Check the identification number if present, located on the circuit board next to the ac connector or on the end of the line filter.



If the number is 9300 or less, check for either of the following identification marks:

- (a) Red line under fuse.
- (b) Red dot on top of capacitors C7, C8 and C9.

If the ID number is 9300 or greater or if the mark is present under the fuse or on each of the three capacitors, proceed with the troubleshooting or repair procedures.

If one of the marks is not present remove the heat sink and check capacitors C7, C8 and C9 for vent mark.

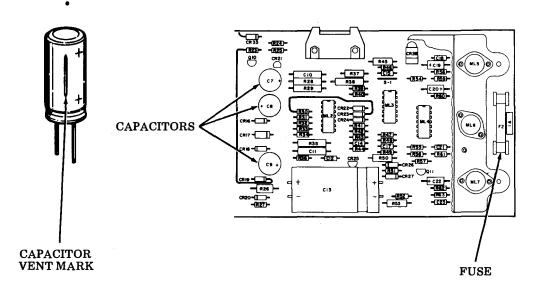
523, 3-4

C. DISASSEMBLY/REASSEMBLY (Contd)

1. 430700 and 430780 Power Supply (Contd)

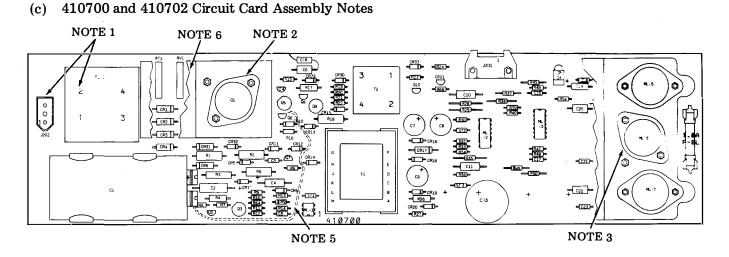
(b) Vented Capacitors (410700 Circuit Card, Issue 4D or earlier) (Contd)

Replace C7, C8 and C9 capacitors if vent mark is not present. Observe proper polarity when replacing.



Mark top of vented capacitors with red dot and draw a red line under fuse (use indelible felt tip marker).

Replacement vented capacitors for this purpose can be obtained at no charge from Teletype Corporation by indicating "No charge per Manual 391" on the order for the 430704 capacitor.



Note 1: Mount FL1 with two-pin side adjacent to connector and bend side tabs on underside toward each other. A minimum of 0.20 inch clearance must be maintained between circuit board and case of filter. Use 131228 insulating washers over mounting tabs, if required.

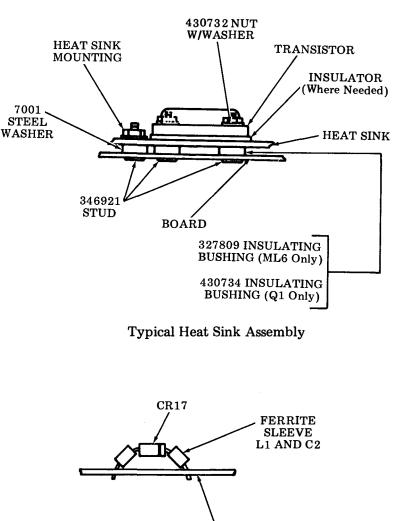
Note 2: Mount the 430710 insulating washer between heat sink and transistor Q1.

Note 3: Use suitable heat sink compound under Q1, ML5, ML6 and ML7. Compound to be applied between insulator and heat sink of Q1 and ML6.

Note 4: Typical diode-sleeve assembly (410702 card assembly).

Note 5: (410700 card assembly) Customer I.D. 9A and earlier: if repair requires replacement of Q1, a grounding path improvement should be provided, on the compoment side of the card assembly, by cutting the circuit path between the emitter of Q6 and the anode of CR12 at a point 1/4" to 3/8" from Q6. An insulated 20 AWG stranded strap must then be connected between the emitter of Q6 and the negative terminal of C1. Add the strap approximately as shown.

Note 6: Install 430739 insulator to cover RV1 and RT1. Align holes with weld nuts on underside of 430723 heatsink bracket.

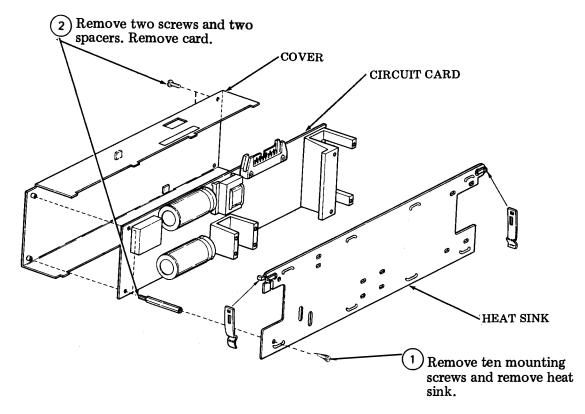


BOARD

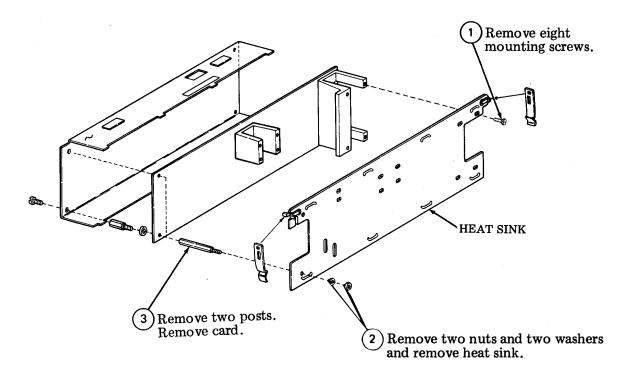
C. DISASSEMBLY/REASSEMBLY (Contd)

2. **430760** Power Supply

(a) 410703 Circuit Card Removal

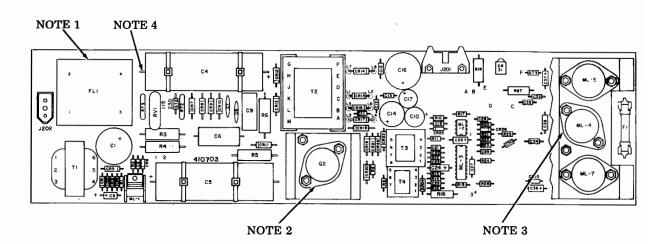


(b) 410704 Circuit Removal



(c) 410703 Circuit Card Assembly Notes

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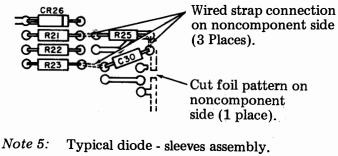
Note 1: Mount FL1 with no-pin side adjacent to connector and bend side tabs on underside toward each other. A minimum of 0.20 inch clearance must be maintained between circuit board and case of filter. Use 131228 insulating washers over mounting tabs, if required.

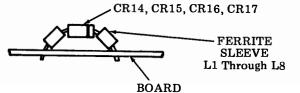
Note 2: Mount the 430710 insulating washer between heat sink and transistor Q2.

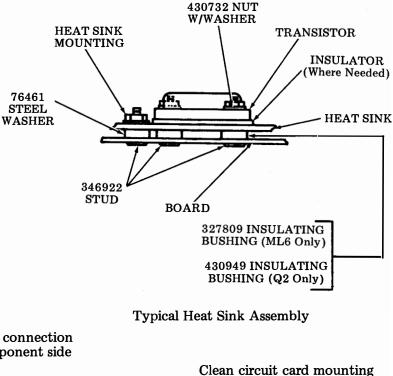
Note 3: Use suitable heat sink compound under Q2, ML5, ML6 and ML7. Compound to be applied between insulator and heat sink of Q2 and ML6.

Note 4: Suitable tubing to cover exposed leads on C4 and C5 (4 places).

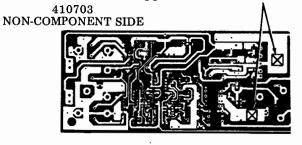
Mounting Procedure for R25 and C30:





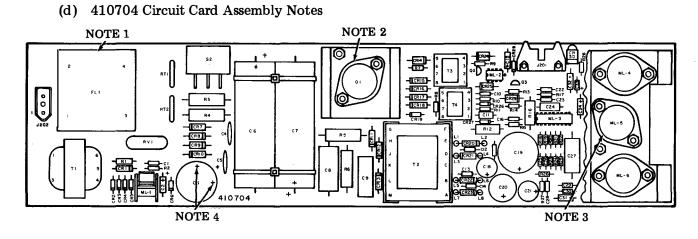


surface with Trichloroethane and adhere 454134 bumpers in approx. area shown.



C. DISASSEMBLY/REASSEMBLY (Contd)

2. 430760 Power Supply (Contd)



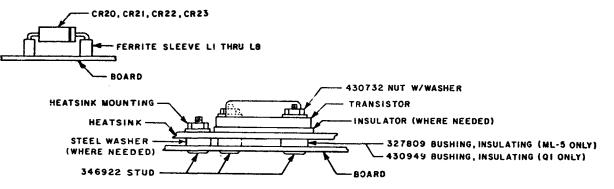
Note 1: Mount FL-1 with two pin sides adjacent to 341964 connector and bend side tabs on underside toward each other. A minimum of .020 clearance must be maintained between circuit board and case of filter.

Note 2: Mount 430710 insulating washer between heat sink and transistor Q1.

Note 3: Suitable heat sink compound under Q1, ML-4, ML-5 and ML-6. Compound to be applied between insulator and heat sink of Q1 and ML-5.

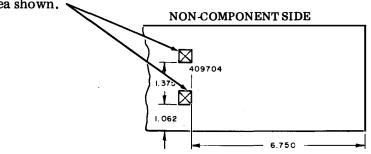
Note 4: Location of positive lead may vary with manufacturer.

Note 5: TYPICAL DIODE - SLEEVES ASSEMBLY



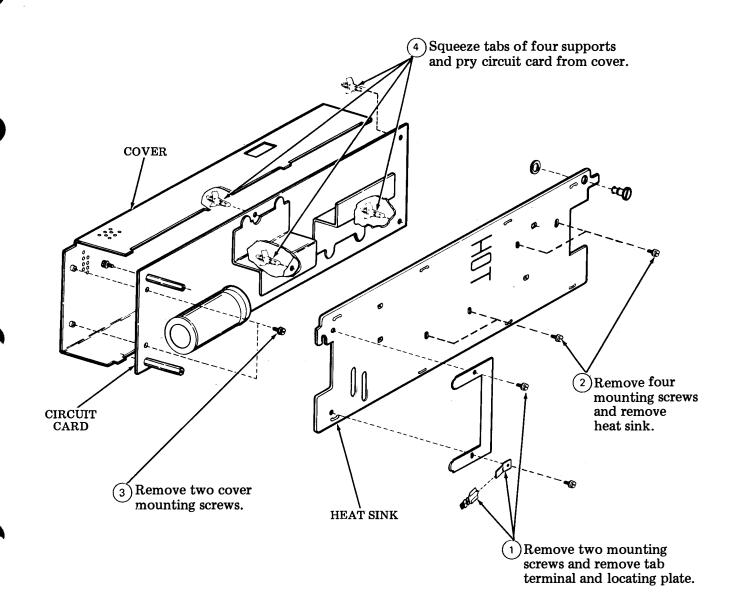
Typical Heat Sink Assembly

Note 6: Clean circuit card mounting surface with trichloroethane and adhere 454134 bumpers in approximate area shown.



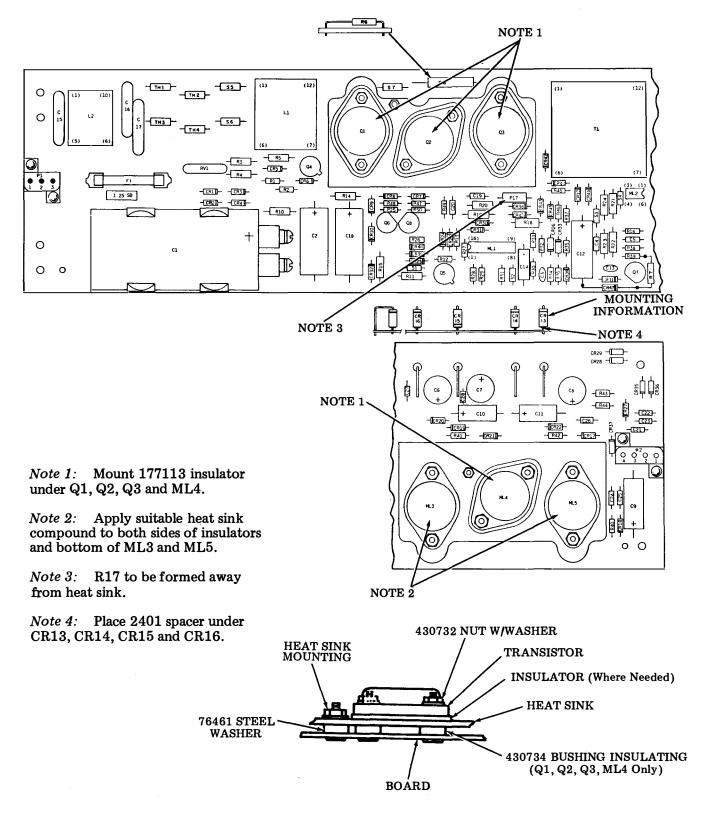
3. 430770 Power Supply

(a) 410701 Circuit Card Removal



C. DISASSEMBLY/REASSEMBLY (Contd)

(b) 410701 Circuit Card Assembly Notes



Typical Heat Sink Assembly

PART 4 - CIRCUIT DESCRIPTIONS AND DIAGRAMS

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A. GENERAL

This part provides circuit descriptions and combined schematic and troubleshooting circuit diagrams for power supplies used with 42, 43 and 45-30 CPS Character Printers.

This part includes the circuit descriptions and circuit diagrams for the 430700, 430760, 430770 and 430780 power supply assemblies.

Waveforms and voltage levels are shown on the diagrams whenever possible to aid in troubleshooting and understanding the circuit theory. Circuit descriptions refer to coordinates on the schematic, ie, (C2) to locate the circuit being described.

For additional troubleshooting information associated with these circuit drawings, refer to PART 2 - TROUBLESHOOTING which includes:

Troubleshooting Charts (430700, 430760 and 430780). Tables for dynamic and static VOM measurements. Illustrated layouts of circuits and physical location of component and connector leads.

For part number identification of components shown on circuit diagrams refer to PART 5 - PARTS.

Most numbers shown on various leads, components, and connectors on the circuit diagrams are not actually marked on the equipment. They are required for identification purposes when referring to other parts of the manual.

Note: When ordering replaceable parts or components, unless otherwise specified, prefix each part number with the letters "TP" (ie, TP410055).

B. CIRCUIT DESCRIPTIONS

430700 and 430780 POWER SUPPLIES 410700 and 410702 CIRCUIT CARDS

OPERATION

The 430700 and 430780 power supplies are of the "Off-the-Line" switching regulator type utilizing a "Ringing Choke" design to accomplish power conversion at a nominal frequency of 20 KHz. This design provides a relatively high power conversion efficiency, and minimizes the size and weight of the supply.

The ac line voltage is directly converted to dc by a bridge rectifier connected directly to the ac input and filtered by a capacitor on the output side of the bridge rectifier. The primary of a power transformer is connected to the dc source in series with a primary switching transistor. In operation, the transistor is driven into conduction for a controlled period of each cycle during which the current in the primary increases. During the remainder of the cycle, the transistor is nonconducting, but the energy stored in the primary inductance is transferred to four secondary windings. The secondaries each contain a semiconductor diode which provides half-wave rectification.

The +5 V, +12 V and -12 V outputs are derived from three separate windings which drive integrated circuit voltage regulators. These regulators are of the linear type.

The +42 V output is derived from the fourth secondary winding. This output is sensed by a feedback circuit which controls the conduction period of the primary switching transistor so that the output is regulated to the correct voltage in response to line and load variations.

430700 and 430780 POWER SUPPLIES 410700 and 410702 CIRCUIT CARDS (Contd)

OPERATION (Contd)

The protective ground is not connected to the primary circuit ground. Care must be exercised during troubleshooting to prevent direct connection of these grounds because this will effectively bypass one of the bridge rectifier diodes and cause full line voltage to be directly applied to another diode in the forward direction. This rectifier and other line components will fail under this condition.

The secondary voltage returns are tied together and directly connected to the protective ground. However, isolation is maintained between the ac line and the secondary circuits.

GENERAL

1. Operating Modes

During normal operation, the 430700 and 430780 power supplies function as a fixed frequency, pulse width modulated switching regulator. However, whenever power is initially applied, the oscillator and control circuitry which are on the secondary side of the main power transformer T1 are not operational. An auxiliary mode of operation is provided which is operational only during start-up while the oscillator and control circuitry are nonoperating. In this auxiliary mode, the primary switching transistor is driven by an extra winding on transformer T1 which is connected such that positive feedback is provided to its base. This results in a blocking oscillator like mode of operation during start-up.

Operation of the power supply in the power-up mode results in energy transfer to the secondary windings so that the oscillator and control circuitry, which are powered from the unregulated voltage which drives the +12 V regulator, will commence operation. With a low secondary voltage, the control circuitry provides a maximum pulse width which is constrained to be slightly less than 50 percent of a cycle. Whenever the oscillator drive has gained sufficient amplitude to reliably drive the primary switching transistor, the blocking oscillator action is automatically terminated and operation continues under oscillator driven control.

2. AC Line Rectifier

The ac to dc rectification occurs through the full-wave bridge consisting of the four diodes CR1, CR2, CR3 and CR4. Capacitor C1 filters the dc.

The anodes of CR3 and CR4 and the negative end of C1 are connected to a common bus for all primary circuits. This bus is not to be confused or connected with any ground bus on the secondary circuits unless the power supply is floated through an isolation transformer. Grounding of the primary bus might cause destruction of diode CR3, as well as thermistor RT1.

3. Blocking Oscillator

Upon initial application of dc voltage to R3 (A6), current flows to charge C2 (B6). The time constant of R3 and C2 delays the start-up until capacitor C1 (G8), is fully charged.

The voltage across C2 biases the base of Q1 (D7), into the active region by applying dc potential through R8 (B7), terminal (J, H) of P2 and diode CR11. This causes current to flow into the base of Q1 tending to turn it on. As Q1 turns on, terminal L of P1 is forced toward primary bus common. Since coil P1 is tightly coupled to P2 an equivalent potential is applied across P2 according to the dot notation shown. R15 (D7), is a base bias resistor for Q1.

A portion of P2 is tapped at J to act as a source to further drive the base of Q1 toward saturation. Regenerative action occurs because of positive feedback driving Q1 into saturation.

Base drive into Q1 is limited by resistor R8. The Q1 collector current ramps up due to the magnetizing inductance of T1. This current is limited by the gain hFE of Q1. For constant current base drive, Q1 remains in saturation until IC exceeds hFE times I_B .

As Q1 comes out of saturation voltage across J-H is reduced, lowering the base drive to Q1. Regenerative action occurs forcing Q1 off. Q1 remains off until the energy in T1 collapses via dumping energy into the secondaries (S1, S2, S3, S4). The cycle then repeats itself until the pulse width modulator mode takes over.

4. Snubbing Circuit

The snubbing network consisting of coil P2 and diodes CR14 (B7) and CR12, clamp the collector of transistor Q1 during turn off to twice the dc supply voltage. During turn off terminal L of P1 exceeds the potential at terminal G due to the inductive kick of the transformer T1. The potential across terminals L-G is mirrored on terminals K-H by observing the dot notation polarity.

Upon turn off terminal K becomes more positive than +Vdc in and is clamped by CR14. Terminal H becomes more negative than the -Vdc bus common. This forces a clamping of coil P2 which reflects to coil P1 due to tight coupling. The voltage on the collector of Q1 is limited to that across P2 or twice V_{IN} . Diode CR7 prevents capacitor C2 from being reversed biased.

OSCILLATOR DRIVEN MODE

1. 20 KHz Square Wave Oscillator

During start-up, the secondaries of T1 receive a limited amount of power which results in an increasing rectified voltage. The oscillator is fabricated from one of the comparitors in ML2 which derives its power from the regulated +12 V supply. As the voltage increases to approximately 4 V, oscillation commences.

If the oscillator output (Pin 2) (H12), has just switched to ground, the voltage at the noninverting input (Pin 5) will be determined by the divider of R35 and R28 in parallel with R32. This voltage is 31 percent of the +12 V supply. The voltage on the inverting input (Pin 4) discharges toward ground at a rate determined by R38 and C11. As this voltage drops to 31 percent of the +12 V supply, the comparator output switches to the high state. Now, the voltage on (Pin 5) is essentially determined by the divider of R28 in parallel with R35 and R32. This voltage is 62 percent of the +12 V supply. The voltage on (Pin 4) charges toward the +12 V supply at a rate determined by R30 and R38 in series, and C11. As this voltage now reaches 62 percent of the +12 V supply, the comparator output (Pin 2) switches to the low state.

Since the comparator switch points are a fixed ratio of the +12 V supply, the frequency will be virtually independent of the actual voltage of the +12 V supply. In fact, from approximately +4 V to +20 V, the frequency and duty cycle are essentially constant.

The ramp generator is fabricated from a second comparator of ML2. The inverting input (Pin 8) of ML2 (H13) is biased to approximately 50 percent of the +12 V supply by a divider composed of R33 and R36. The output of the 20 KHz square wave oscillator is connected to the noninverting input (Pin 9). Whenever the oscillator output is low, the output (Pin 14) is held in the low state. The voltage on capacitor C10 is held low during this time.

Whenever the oscillator output goes to the high state, the output of the ramp generator is unclamped. The voltage on C10 begins to charge toward the +12 V supply by means of resistor R29. The voltage reaches approximately 3.5 V during the time that the oscillator output is high. Whenever the oscillator output goes to the low state, C10 is discharged and the ramp voltage goes to a few tenths of a volt above ground.

OSCILLATOR DRIVEN MODE (Contd)

2. Pulse Width Modulator

A third section of ML2 is used for a pulse width modulator. The output of the ramp generator is connected to the noninverting input (Pin 11) (H14) by means of resistor R39. The inverting input (Pin 10) is connected to a divider network consisting of R47 and R48 which derives a bias of approximately 0.6 V from the +12 V supply.

In the absence of any output from (Pin 9) of ML3 (F12), the bias voltage of 0.6 V appears on (Pin 10) of ML2. Consequently, whenever the ramp generator output is low, the pulse width modulator output (Pin 13) will be low shunting any current flowing through R25. Whenever the ramp generator output exceeds the bias voltage, the pulse width modulator will go to a high state. Any current flowing through R25 (early versions) R68 (late versions) will now be available to drive the base of transistor Q10 (D3).

Resistor R25 (R68) is connected in series with 4-layer diode CR21 (G15). This diode is nonconducting until the +12 V supply exceeds approximately 8 V, at which point the diode triggers into conduction with a drop of approximately 1 V. During start-up, even though the oscillator is running and the pulse width modulator is producing drive pluses, transistor Q10 will not receive drive pulses until CR21 becomes conducting.

Whenever an output is produced on (Pin 9) of ML3 that exceeds the 0.6 V bias, the pulse width of the output on (Pin 13) of ML2 will be reduced. The pulse width modulator output will be in the high state for the time that the ramp generator output exceeds the voltage produced on (Pin 9) of ML3.

Resistor R40 is connected between the ramp generator output and the noninverting input to provide hysteresis and snap action switching. Resistor R24 provides a base leakage path for transistor Q10.

3. Voltage Reference and Error Amplifier

The voltage reference and error amplifier is contained in ML3 (G11), a type 723 precision regulator. The voltage reference, V_{REF} (Pin 6), is nominally 7.15 V with a 5 percent tolerance. This voltage is applied to a precision divider consisting of R37 and R45 to provide a 3.57 V reference which is applied to the inverting input (Pin 4) of the error amplifier.

The +42 V rectified dc output is connected to a precision divider consisting of R49 and R50 (G10). The resulting voltage is applied to the noninverting input (Pin 5) of the error amplifier. In operation, the voltage at (Pin 5) is very close to that at (Pin 4). Frequency compensation of the error amplifier is accomplished by connection of capacitor C15 (G12), between the compensation terminal (Pin 13) and the inverting input (Pin 4).

The dc gain of the error amplifier, ML3, is utilized to produce the control signal at (Pin 9). Gain of the error amplifier is reduced by use of negative feedback from the direct output at (Pin 10) through resistor R46. Capacitor C17 (F13), is used to bypass any high frequency noise in proximity to the error amplifier.

4. Primary Power Conversion

As previously noted, the 20 KHz oscillator will commence operation and produce **drive** pulses to the base of transistor Q10 whenever the +12 V supply exceeds approximately 8 V. At this point, the pulse transformer T2 (C3), in the collector of Q10 will be driven so as to produce a positive pulse of similar duration on its secondary. This pulse is connected through resistor R18 (C7), and diode CR10 to the base of the primary switching transistor, Q1.

The positive drive on the base of Q1 causes current to flow in the collector of Q1 and the primary winding (P1) of transformer T1. The current increases, linearly during the duration of the pulse, from its initial value to its final value which is dependent upon the pulse width as well as the dc supply voltage. Diode CR13 (C7), effectively prevents Q1 from reaching full saturation, reducing the storage time for Q1.

The positive pulses are also connected through diode CR9 (D4), which rectifies the signal to produce a dc signal on capacitor C4 and bleeder resistor R13. When the power supply begins operating in the oscillator driven mode, the dc signal is connected through diode CR8 and resistor R9, to the base of transistor Q7 (B7). The collector of Q7 is connected to the feedback winding used to provide the blocking oscillator action. Turning Q7 on will short the signal produced by the feedback winding and effectively inhibit blocking oscillator action. This control is automatically transferred from the start-up mode to the oscillator driven mode.

Whenever the drive to the base of Q10 is shunted by the pulse width modulator, the drive pulse is terminated. The collector of Q10 rises from the saturated value of Q10 to a voltage above the +16 V supply. This results in a negative pulse on the secondary of T2. This pulse is connected through resistor R22 (D6), to the base of transistor Q5. Transistor Q5 is turned on which effectively grounds the base of Q1. The stored base charge in Q1 is discharged through Q5 resulting in rapid turnoff of Q1.

When Q1 turns off, the energy which was stored in the magnetic core of T1, is transferred to the secondary windings. Each winding is driven in proportion to its relative turns ratio.

5. Feedback Regulation

As dc line power is transferred to the secondary circuits, the rectified secondary voltages increase. The +42 V supply is sensed by means of divider R49 and R50 (G10), and compared in the error amplifier with the voltage reference established by divider R37 and R45. Whenever the sensed voltage exceeds the reference voltage, the error amplifier output (Pin 9) is increased which has the effect of reducing the pulse width supplied to drive Q1. As a result, the net energy transferred to the secondary is reduced. This also causes the rectified secondary voltages to decrease. Consequently, the +42 V supply is regulated against line and load changes. In addition, the remaining three secondaries are also regulated against line changes and to some extent, load changes, to the degree that they are reflected in the +42 V supply voltage.

The +42 V supply is derived from a secondary winding of T1. The voltage on winding A-E is half-wave rectified by diode CR17 (C10), and filtered by capacitor C13. A bleeder resistor R26 is provided to discharge C13.

The purpose of the optical coupler is to deactivate the blocking oscillator mode of operation following a normal start-up sequence, or upon detection of a +42 V overvoltage condition. Overvoltage is detected by diode CR20 (C12), resistor R27, and ML1 optical isolator diode. Under light loads, the secondary voltages may substantially exceed their ratings during this condition. The overvoltage protective circuitry which functions by inhibiting the clock is not capable of inhibiting the blocking oscillator action.

Whenever the +42 V supply voltage exceeds approximately 47 V, zener diode, CR20 will conduct and drive the LED in optical isolator ML1. Resistor R27 limits the current through the diode.

OSCILLATOR DRIVEN MODE (Contd)

5. Feedback Regulation (Contd)

The phototransistor in ML1 (B4), in conjunction with transistor Q3 forms a latch on the ac line side of the power supply. Whenever the latch is off, a voltage appears on the emitter of Q3 which is the result of a fixed drop across the zener diode CR5 (B4), and a divider consisting of R1 and R6. Capacitor C3 filters noise appearing on the emitter. As secondary voltages are developed by blocking oscillator action, a transition to the oscillator driven mode generates positive pulses at T2 transformer terminal 4, which are coupled to Q1 base and to the phototransistor (Pin 6), through CR9, R10 and R11. The phototransistor conducts current through resistor R12 which is connected to the base of Q3. This base current causes collector current to flow through Q3 which, in turn, drives the base of the phototransistor by means of resistor R11. Transistor Q3 becomes latched so that in the event of a failure in the oscillator control circuit, transistor Q7 will continue to be driven, which prevents the blocking oscillator from restarting. Resistor R14 provides base stabilization for the phototransistor, and capacitor C5 filters noise transients to prevent spurious triggering of the latch.

Zener diode CR5 is provided to permit the latch to clear whenever the rectified primary dc voltage drops below approximately 50 V. This allows the power supply to automatically restart under the blocking oscillator mode of operation if the oscillator driven mode has also become inoperative.

6. Primary Circuit Overcurrent Protection

A resistor, R4 (D7), in the emitter of the primary switching transistor, Q1, senses the current conducted during each pulse drive period. If this current should exceed a safe level, the base drive current is shunted for the remainder of the drive pulse.

The voltage developed on R4 is applied through resistor R19 (D3), to capacitor C6 which acts to filter spurious transients, to R17 which is in series with the base of transistor Q8, and to the base of transistor Q4. Whenever the voltage developed is high enough to cause Q8 to conduct sufficient current through the collector resistor, R20, which is connected through diode CR15 to the drive pulse transformer T2, to bias transistor Q9 into conduction, a regenerative action is initiated. This allows current to flow through the emitter resistor, R21, of Q9. The current drives both the base of Q8 and the base of Q4. Whenever Q4 conducts, the base drive current to Q1 is shunted to the primary common, effectively terminating the primary switching transistor current pulse for the cycle. Whenever the drive pulse from transformer T2 terminates, transistors Q8, Q9 and Q4 are returned to their nonconducting state.

7. Primary Circuit Overvoltage Protection

In the event that a transient spike occurs on the ac line that exceeds the normal voltage range, circuitry has been provided which will maintain the primary switching transistor in the nonconducting state even through base drive pulses are being generated. This protection is accomplished by shunting the oscillator drive pulses during the transient.

Zener diode CR6 (B6), cathode is connected to the primary dc power, and anode to resistor R2. Whenever the dc voltage is high enough to exceed the zener diode voltage, current flows to the base of transistor Q2 by means of resistor R7, and the base of Q6 by means of resistor R16. Base bias resistor R5 serves to bypass leakage current for both Q2 and Q6.

LOGIC VOLTAGES

1. +5 V Supply

The +5 V supply is derived from a secondary winding of T1. The voltage on winding F-M is half-wave rectified by diode CR16 (A10), and filtered by capacitors C7 and C18. This unregulated voltage, +9 V, is applied to the base connection (B) of a linear regulator, ML5, which is a elf-contained three terminal integrated circuit located on a common heat sink with ML6 and ML7. A capacitor, C19, on the output (E) of the regulator filters high frequency load transients.

2. +12 V Supply

The +12 V supply is derived from a secondary winding of T1. The voltage on winding S2 is half-wave rectified by diode CR19 (E10), and filtered by capacitors C9 and C23. This unregulated voltage, +16 V, is applied to the base connection (B) of a linear regulator, ML7, which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML6. A capacitor, C22, on the output (E) of the regulator filters high frequency load transients. The +16 V supply is also used to drive the error amplifier.

3. -12 V Supply

The -12 V supply is derived from a secondary winding of T1. The voltage on winding S3 is half-wave rectified by diode CR18 (B10), and filtered by capacitors C8 and C21. This unregulated voltage, -16 V, is applied to the collector connection (C) of a linear regulator, ML6, which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML7. A capacitor, C20, on the output (E) of the regulator, filters high frequency load transients.

4. Output Voltage Indicator

Early Design

Each dc output voltage has a divider network which senses the output level. The sensed output level is compared with a voltage reference derived by a divider network composed of R56 and R61 from the 7.15 V reference voltage, V_{REF} , available from ML3. The comparison is performed using four comparators in ML4 (B15).

The +5 V output voltage sense divider is composed of R58 and R59. The +12 V output divider is composed of R62 and R63. The +42 V supply is sensed by a divider composed of R52 and R53. The -12 V supply is sensed by a divider composed of R55 and R60. These sense voltages are connected to (Pins 11, 7, 5 and 8) respectively of ML4. The voltage reference is connected to (Pins 4, 6, 9 and 10).

The outputs of each comparator (Pins 1, 2, 13 and 14) are connected together. Each comparator will go to a high state on the output whenever its sensed input exceeds the reference voltage. If all four comparator outputs are in the high state, then the current which flows through resistor R54 from the +16 V supply will be available to drive the LED indicator, CR28. If <u>any</u> output voltage should fail, its associated comparator will go to a low state, shunting the current drive to CR28. Note that the sense divider for the +42 V supply is located on the load side of the fuse.

Late Design

A LED indicator will be on whenever +16 V from the output transformer T1, B-C is present.

FAULT PROTECTION ON SECONDARY

1. Short Circuit Protection

The +5 V, +12 V and -12 V supply outputs are protected against short circuits to ground by means of the current limiting characteristics inherent in the integrated circuit voltage regulator which is in each of these outputs. Fault currents are limited to approximately 1.5 amperes. Whenever the fault is removed, the output voltage will either recover or shut off.

These regulators are also thermally protected so that in the event that their power dissipation in conjunction with the ambient temperature exceeds their limit, automatic shutdown occurs. Whenever the internal temperature decreases to a safe level, the device will reset and restore the output voltage.

The +42 V supply is protected against overloads on the output by means on a 1 ampere fast blow fuse, F1.

2. Overvoltage Protection (Early Design Only)

Each secondary output voltage has an overvoltage sense circuit which will cause the power supply to shut down whenever an overvoltage is detected on an output. This is accomplished by means of a voltage comparator in integrated circuit ML2 which clamps the 20 KHz square wave oscillator output to the low state, preventing the generation of drive pulses to the primary switching transistor, Q1.

The inverting input (Pin 6) (J12), of the comparator is biased by the divider network consisting of R33 and R36 to approximately one-half the voltage of the +12 V supply. The noninverting input (Pin 7) is normally biased to the voltage of the +12 V supply by means of R34. An SCR, CR25 (J11), is also connected to (Pin 7).

A zener diode, CR22 (J10), is connected to the +5 V supply in series with current limiting resistor, R43, and to the SCR gate bias resistor R44. Whenever the +5 V supply voltage reaches a level sufficient for the gate voltage to turn on the SCR, (Pin 7) of the comparator is driven below the bias voltage on (Pin 6) resulting in a low state on the output, (Pin 1). This condition is maintained until the +12 V supply drops so low that the oscillator is no longer operational. Capacitor C14 acts as a filter for high frequency transients. Capacitor C12 provides a short time delay on oscillator operation during start-up as well as enhances triggering of the SCR. Resistor R31 is intended to provide snap action during start-up.

The +12 V supply is sensed in a similar manner by zener diode CR23 and resistor R42.

The +42 V supply is detected in the same manner by zener diode CR24 and resistor R41.

The -12 V supply is also sensed, but in a slightly different manner. A zener diode CR27 is connected directly to the base of transistor Q11. Normally, Q11 is biased into saturation conduction by resistor R51 which is directing connected to the +16 V supply. Whenever the zener diode voltage is substantially exceeded, the base bias current is shunted so that Q11 becomes nonconducting. While Q11 is saturated, its collector voltage is held low. However, whenever the transistor becomes unsatureated, the collector pull-up resistor, R57, connected to +16 V will raise the collector voltage. This voltage is applied through diode CR26 to the gate of CR25, causing the SCR to conduct.

430760 POWER SUPPLY

OPERATION

The 430760 PSU is of the "Off-the-Line" switching regulator type, utilizing a "Flyback" design to accomplish power conversion at a nominal switching frequency of 40 KHz.

When strapped for 230 Vac input, the ac line voltage is directly converted to dc by the bridge rectifier connected to the ac input and filtered by a capacitor arrangement on the output side of the bridge rectifier.

When strapped for 115 Vac input, the ac line voltage is converted to a FWR (Full-Wave-Rectified) dc voltage via a voltage doubler circuit, and filtered. This input dc voltage has about the same amplitude (320 Vdc) whether the PSU is strapped for 115 Vac or 230 Vac; from this point on, the operation does not depend on whether the unit is strapped for 115 Vac or 230 Vac.

The primary side of a switching power transformer is connected in series with the dc input voltage and the collector of the switching power transistor. In operation, the transistor is driven into conduction for a controlled period of each cycle, during which time the current in the primary winding increases. During the remainder of the cycle the transistor is nonconducting, but the energy stored in the inductance of the primary winding is transferred to the secondary windings. The secondaries contain diodes which provide half-wave rectification.

Three rectified secondary winding taps develop unregulated dc voltages of about +9 V, +17 V and -17 V. These unregulated voltages are the inputs to three linear voltage regulators.

The +42 V output is derived from the other secondary winding. This output is sensed by a feedback circuit which controls the conduction time of the switching power transistor so that the output is regulated to the correct voltage.

Caution: The protective ground is not connected to the primary circuit common. Care must be exercised during trouble shooting to prevent direct connection of the ground and the common, since this would effectively short one of the rectifier diodes during one half cycle. This rectifier and other components will fail under this condition.

The secondary output voltage grounds are tied together and are directly connected to the protective ground.

GENERAL

Operating Modes

During normal operation, the 430760 power supply functions as a fixed frequency, pulse width modulated switching regulator. However, when ac power is initially applied, the pulse width modulator and the proportional drive receive their power from a "Start-Transformer". This is a small linear step-down transformer, which provides about 21 Vdc (after bridge rectification and filtering) to the input of a three terminal 5 V regulator. The 5 V regulator is "Offset" to provide about 10.3 Vdc to the V Start connection. Once all logic voltages and the +42 V is within tolerance, the +12 V logic output will provide power to the control circuitry. The start power circuitry is in an idle state during normal operation.

The "Start Transformer" is connected in a unique manner in the voltage doubler circuit. When the PSU is strapped for 115 Vac, the primary side of the "Start Transformer" is connected directly across the ac input lines. In the 230 Vac operating mode the "Start Transformer" is connected to the lower half of the "Voltage-Doubler-Circuit", and therefore has 115 Vac across the primary side.

410703 CIRCUIT CARD POWER-UP MODE

1. AC Line Rectifier

230 Vac strap: AC to dc rectification occurs through the full-wave bridge consisting of four diodes CR7, CR8, CR9 and CR10. Capacitors C4 and C5 (series connection) filter the rectified voltage, and resistors R3 and R4 serve as voltage equalizers (across C4 and C5), and bleeder resistors. Capacitors C7 and C8 are high frequency filters.

115 Vac strap: AC to dc rectification is through a full-wave rectified voltage doubler circuit. In this option CR7 and CR8 are always reversed biased. During a positive half-cycle, current flows through RT1 and CR9, and charges filter capacitor C5; CR10 is reverse biased. During a negative half-cycle, CR9 is reverse biased, and current through CR10 charges filter capacitor C4. The dc voltages across C4 and C5 are in series, therefore doubling and rectified line voltage.

2. Start Voltage

230 Vac option: The function of transformer T1 is to provide the start-up power needed to drive the pulse width modulator IC (ML3) and the clock driver IC (ML2). One side of the primary is connected to the junction of C4 and C5, the other side is connected to the junction of CR9 and CR10. The alternating voltage across the primary side of T1 is <u>not sinusoidal</u>, and is a symmetrial voltage of about 320 V peak-to-peak.

115 Vac option: With the 115 Vac strap option, the ac input line voltage is directly applied to the primary of T1.

V Start Developing: The secondary voltage of T1 is converted to dc by a bridge circuit (CR1, CR2, CR3, CR4), and filtered by an electrolytic filter capacitor (C1). This unregulated dc voltage is used as the input to a +5 V regulator IC (ML1), which is offset-biased to provide about +11 V at the output terminal. The offset-biased is accomplished by R2 and R1. Blocking diode CR6 prevents the +12 V logic voltage from being applied to the ML1 output terminal during normal operation.

Zener diode CR5 protects ML1 against high input voltage transients.

3. dV/dt Circuit Snubber

The snubber network consisting of R5, C6 and CR11 prevents the collector voltage of Q2 from rising too rapidly while collector current is still present. When Q2 is being turned off and the collector voltage rises, diode CR11 becomes forward biased, and capacitor C6 begins to charge. When the collector voltage of Q2 decreases, C6 discharges through R5.

4. dI/dt Circuit Snubber

The function of CR13, C9, R6 and CR12 is to limit the reverse voltage developed across M and G of T2 during "kickback". Reverse kickback voltages below 190 V are dampened by the R6, C9 network which is in parallel with the zener diode CR12.

5. Current Limiting Circuit

Current sensing is accomplished through the use of current transformer T4. The voltage developed across the primary side of T4 is reflected to the secondary side at 5 times its primary amplitude. Cycle by cycle current limiting is initiated when the rectified filtered waveform at the junction of R15 and C25 is about 4.5 V. This corresponds to a Q2 collector current of about 3A.

6. Proportional Drive Circuit

The base-drive circuit to control the power switching transistor Q2, is of the active turnon/turnoff type. The "Set" current pulse is applied to terminals (1 through 4) of T3. When reflected to the primary side, the stepped up current pulse from terminals (5 through 6) of T3 initially drives the base of Q2, which then latches to a base current of (6 turns/22 turns) times IE(Q2). The negative "Reset" current pulse, rapidly "Unlatches" the base of Q2, and "Resets" the core of transformer T3.

The base drive circuit uses a modified baker clamp (CR18, CR21, CR22, CR23, R8) to prevent the collector of transistor Q2 from going into saturation, thereby keeping the switching time of Q2 to a minimum.

Diode CR19 and zener diode CR20 prevent the base of transistor Q2 from going more than 7 V negative with respect to the emitter.

The width and the amplitude of the "Set" current pulse is determined by CR25, C19 and R10. The values of R17 and C28 determine the width and the magnitude of the "Reset" current pulse.

Diode CR26 prevents the input of the clock driver from going more than 0.7 V negative. Resistor R20 "swamps" the input of the clock driver, and provides a bleeder path for C28.

PULSE WIDTH MODULATOR IC

1. Reference Regulator

An on-chip regulator, trimmed to within ± 1 percent, is the stabilized power source for all the internal circuitry, with the exception of the current limit comparator, and the output driver.

2. Error Amplifier

The reference regulator output, V_{REF} , is externally connected to the + input (noninverting) of the error amplifier (Pin 1).

The +42 V rectified dc output is connected to a precision divider consisting of R21 and R22. The resulting voltage is applied through R23 to the - input (inverting) (Pin 2) of the error amplifier.

During normal operation, the voltage at (Pin 2) of the PWM IC is very close to that at (Pin 1). Frequency compensation of the error amplifier is accomplished by a feedback network consisting of R23, R11, C20, R12, C23 and C22.

3. Sawtooth Oscillator

The sawtooth oscillator is programmed for a frequency of about 80 KHz by resistor R18 and capacitor C27. Since no "dead time" is allowed, the RD (R dead time) connection (Pin 11) is to ground. The switching frequency is one-half the oscillator frequency.

4. Current Sensing

The invert input (-) of the current limit comparator is biased by a percision divider comprised of R13 and R14. The noninvert input (+) is connected to the junction of R15 and C25. Pulse processing logic, inherent in the PWM permits pulse-by-pulse current limiting, and prevents double pulsing.

5. Undervoltage Lockout

The pulse width modulator IC is prevented from operating (0 percent duty cycle) by the undervoltage lockout circuitry when the $+V_{IN}$ voltage (Pin 17) is below 8.0 V.

PULSE WIDTH MODULATOR IC (Contd)

6. Primary Power Conversion

After power has been applied, the pulse width modulator IC will increase the pulse width (duty-cycle) from a minimum value as part of its slow-start feature.

When output B (Pin 16) of the pulse width modulator goes from low to high, the ML2-7 clock driver output goes low. This low going transient is coupled through R10, C19 to (Pin 1) of transformer T3 and setting the voltage at (Pin 1) to around +2 V. Since the output of the other clock driver (Pin 7) has not felt any change, the instantaneous voltage across terminals 1 and 4 of T3 is about 8 V with (Pin 4) being more positive. Observing the dot notation, the reflected voltage across terminal (5 through 6) is about 2.7 V. This voltage will forward bias diodes CR23, CR22, and CR18, and will drive a large base current into transistor Q2, rapidly turning it on.

When output B (Pin 16) of the pulse width modulator goes from high to low, the clock driver output (Pin 7) goes to about +11 V, applying instantly about +10.5 V to (Pin 1) of T3, and a high to (Pin 4) of the other clock driver. The output of this clock driver (Pin 5) is driven low and pulls (Pin 4) to T3 low. This voltage across (1 through 4) of T3 is reflected across (5 through 6) of T3 with terminal 5 being more negative. This negative voltage pulse forward biases diode CR21 and rapidly removes the base current from Q2, turning it off.

Zener diode CR20 and diode CR19 limit the base-emitter voltage from becoming more than 7 V negative.

LOGIC VOLTAGES

1. +5 V Supply

The +5 V supply is derived from a tap on the secondary winding of power transformer T2. The voltage on winding S1 is half-wave rectified by diode CR17 and filtered by capacitors C14 and C11. This unregulated voltage, +9 V, is applied to the base connection (B) of a linear regulator, ML5, which is a self-contained three terminal integrated circuit located on a common heat sink with ML6 and ML7.

Capacitors C33 and C37 are connected as close as possible across the input (B) and the output (E) terminals of the regulator to filter high frequency load transients.

2. +12 V Supply

The +12 V supply is derived from a secondary winding of T2. The voltage on winding S2 is half-wave rectified by diode CR16, and filtered by capacitors C18 and C13. This unregulated voltage, +17 V, is applied to the base connection (B) of a linear regulator, ML7, which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML6.

Capacitors C34 and C36 are connected as close as possible across the input (B) and the output (E) terminals of the regulator to filter high frequency load transients.

Diode CR35 prevents the start voltage V-start from being applied to the output of ML7 during start-up.

3. -12 V Supply

The -12 V supply is derived from a secondary winding of T2. The voltage on winding S3 is half-wave rectified by diode CR15 and filtered by capacitors C15 and C17. This unregulated voltage, -17 V, is applied to the collector connection (C) of a linear regulator, ML6 which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML7, but electrically isolated from the heat sink.

Capacitors C35 and C38 are connected as close as possible to the input (C) and the output (E) of the regulator to filter high frequency load transients. Note the ground polarity connection of C17 and C38.

4. +42 V Supply

The +42 V supply is derived from a separate secondary winding of T2. The voltage on winding S4 is half-wave rectified by diode CR14 and filtered by capacitors C16 and C12.

Resistor R19 establishes the minimum load for the +42 V output.

The 1.0A slow blow fuse prevents printer head damage, if a printer head driver transistor shorts on the logic board.

The LED indicator (CR31) is "ON", whenever the fused +42 V output is present. Resistor R27 limits the current through the diode.

Additional filtering of the +42 V output is provided by a 1500uf or 2400uf capacitor on the logic board.

5. Voltage Sense

Feedback to the input of the error amplifier of the pulse width modulator is provided by a precision resistor divider consisting of R21 and R22. This voltage is fed through R23 to the negative error input of the pulse width modulator, and is then compared to the V_{REF} voltage at the positive error input.

An internally derived correction voltage adjusts the pulse width of the output signal, such that the compared voltage difference is minimum.

410704 CIRCUIT CARD

POWER-UP MODE

1. AC Line Rectifier

230 Vac selected: AC to dc rectification occurs through the full-wave bridge consisting of four diodes CR7, CR8, CR9 and CR10. Capacitors C7 and C6 (series connection) filter the rectified voltage, and resistors R3 and R4 serve as voltage equalizers (across C7 and C6), and bleeder resistors. Capacitors C4 and C5 are high frequency filters.

115 Vac selected: AC to dc rectification is through a full-wave rectified voltage doubler circuit. In this option CR7 and CR8 are always reversed biased. During a positive half-cycle, current flows through RT1 and CR10, and charges filter capacitor C6; CR9 is reverse biased. During a negative half-cycle, CR10 is reverse biased, and current through CR9 charges filter capacitor C7. The dc voltages across C6 and C7 are in series, therefore doubling and rectifying line voltage.

2. Start Voltage

230 Vac selected: The function of transformer T1 is to provide the start-up power needed to drive the pulse width modulator (ML3) and the clock driver IC (ML2). One side of the primary is connected to the junction of C6 and C7, the other side is connected to the junction of CR9 and CR10. The alternating voltage across the primary side of T1 is <u>not sinusoidal</u>, and is a symmetrical voltage of about 320 V peak-to-peak.

410704 CIRCUIT CARD (Contd)

POWER-UP MODE (Contd)

2. Start Voltage (Contd)

115 Vac selected: With the 115 Vac strap option, the ac input line voltage is directly applied to the primary of T1.

V Start Developing: The secondary voltage of T1 is converted to dc by a bridge circuit (CR5, CR2, CR3, CR4), and filtered by an electrolytic filter capacitor (C3). This unregulated dc voltage is used as the input to a +5 V regulator IC (ML1), which is offset-biased to provide about +11 V at the output terminal. The offset-biased is accomplished by R2 and R1. Blocking diode CR6 prevents the +12 V logic voltage from being applied to the ML1 output terminal during normal operation.

Zener diode CR1 protects ML1 against high input voltage transients.

3. dV/dt Circuit Snubber

The snubber network consisting of R5, C8 and CR11 prevents the collector voltage of Q1 from rising too rapidly while collector current is still present. When Q1 is being turned off and the collector voltage rises, diode CR11 becomes forward biased, and capacitor C8 begins to charge. When the collector voltage of Q1 decreases, C8 discharges through R5.

4. dI/dt Circuit Snubber

The function of CR13, C9, R6 and CR12 is to limit the reverse voltage developed across M and G of T2 during "kickback". Reverse kickback voltages below 190 V are dampened by the R6, C9 network which is parallel with the zener diode CR13.

5. Current Limiting Circuit

Current sensing is accomplished through the use of current transformer T4. The voltage developed across the primary side of T4 is reflected to the secondary side at 5 times its primary amplitude. Cycle by cycle current limiting is initiated when the rectified filtered waveform at the junction of R15 and CR16 is about 4.5 V. This corresponds to a Q1 collector current of about 3A.

6. Proportional Drive Circuit

The base-drive circuit to control the power switching transistor Q1 is of the active turnon/turnoff type. The "Set" current pulse is applied to terminals (1 through 4) of T3. When reflected to the primary side, the stepped up current pulse from terminals (5 through 6) of T3 initially drives the base of Q1, which then latches to a base current of (6 turns/22 turns) times IE(Q1). The negative "Reset" current pulse rapidly "Unlatches" the base of Q1 and "Resets" the core of transformer T3.

The base-drive circuit uses a modified baker clamp (CR14, CR17, CR18, CR19, R7) to prevent the collector of transistor Q1 from going into saturation, thereby keeping the switching time of Q1 to a minimum.

Diode CR16 and zener diode CR15 prevent the base of transistor Q1 from going more than 7 V negative with respect to the emitter.

The width and the amplitude of the "Set" current pulse is determined by CR25, C10 and R10. The values of R14 and C11 determine the width and the magnitude of the "Reset" current pulse.

Transistor Q3, Schottky diode CR29 and resistor R13 improve the "turnoff" characteristic of the directly driven (from the PWM) clock driver.

Transistor Q2, Schottky diode CR24 and resistor R9 improve the "turnoff" characteristic of the other clock driver.

PULSE WIDTH MODULATOR IC

1. Reference Regulator

An on-chip regulator, trimmed to within ± 1 percent, is the stabilized power source for all the internal circuitry, with the exception of the current limit comparator, and the output driver.

2. Error Amplifier

The reference regulator output, V_{REF} , is externally connected to the + input (noninverting) of the error amplifier (Pin 1).

The +42 V rectified dc output is connected to a precision divider consisting of R26 and R23. The resulting voltage is applied through R24 to the - input (inverting) (Pin 2) of the error amplifier.

During normal operation, the voltage at (Pin 2) of the PWM IC is very close to that at (Pin 1). Frequency compensation of the error amplifier is accomplished by a feedback network consisting of R24, R18, C25, R19, C26, C28 and R27.

3. Sawtooth Oscillator

The sawtooth oscillator is programmed for a frequency of about 80 KHz by resistor R25 and capacitor C24. Since no "dead time" is allowed, the RD (R dead time) connection (Pin 11) is to ground. The switching frequency is one-half the oscillator frequency.

4. Current Sensing

The invert input (-) of the current limit comparator is biased by a precision divider comprised of R20 and R21. The noninvert input (+) is connected to the junction of R15 and C16. Pulse processing logic, inherent in the PWM, permits pulse-by-pulse current limiting, and prevents double pulsing.

5. Undervoltage Lockout

The pulse width modulator IC is prevented from operating (0 percent duty cycle) by the undervoltage lockout circuitry when the $+V_{IN}$ voltage (Pin 17) is below 8.0 V.

6. Primary Power Conversion

After power has been applied, the pulse width modulator IC will increase the pulse width (duty-cycle) from a minimum value as part of its slow-start feature.

When output B (Pin 16) of the pulse width modulator goes from low to high, the ML2-5 clock driver output goes low. This low going transient is coupled through CR29, R10, C10 to (Pin 1) of transformer T3 and setting the voltage at (Pin 1) to around +2 V. Since the output of the other clock driver (Pin 7) has not felt any change, the instantaneous voltage across terminals 1 and 4 of T3 is about 8 V with (Pin 4) being more positive. Observing the dot notation, the reflected voltage across terminal (5 through 6) is about 2.7 V. This voltage will forward bias diodes CR17, CR18 and CR19, and will drive a large base current into transistor Q1 rapidly turning it on.

410704 CIRCUIT CARD (Contd)

PULSE WIDTH MODULATOR IC (Contd)

6. Primary Power Conversion (Contd)

When output B (Pin 16) of the pulse width modulator goes from high to low, the clock driver output (Pin 5) goes to about +11 V, applying instantly about +10.5 V to (Pin 1) of T3, and a high to (Pin 2) of the other clock driver. The output of this clock driver (Pin 7) is driven low and pulls (Pin 4) to T3 low. This voltage across (1 through 4) of T3 is reflected across (5 through 6) of T3 with terminal 5 being more negative. This negative voltage pulse forward biases diode CR21 and rapidly removes the base current from Q1 turning it off.

Zener diode CR15 and diode CR16 limit the base-emitter voltage from becoming more than 7 V negative.

LOGIC VOLTAGES

1. +5 V Supply

The +5 V supply is derived from a tap on the secondary winding of power transformer T2. The voltage on winding S1 is half-wave rectified by diode CR23 and filtered by capacitors C14 and C20. This unregulated voltage, +9 V, is applied to the base connection (B) of a linear regulator, ML6, which is a self-contained three terminal integrated circuit located on a common heat sink with ML4 and ML5.

Capacitors C30 and C31 are connected as close as possible across the input (1) and the output (2) terminals of the regulator to filter high frequency load transients.

2. +12 V Supply

The +12 V supply is derived from a secondary winding of T2. The voltage on winding S2 is half-wave rectified by diode CR22 and filtered by capacitors C13 and C21. This unregulated voltage, +17 V, is applied to the input connection (1) of a linear regulator, ML4, which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML6.

Capacitors C32 and C33 are connected as close as possible across the input (1) and the output (2) terminals of the regulator to filter high frequency load transients.

Diode CR28 prevents the start voltage V-start from being applied to the output of ML4 during start-up.

3. -12 V Supply

The -12 V supply is derived from a secondary winding of T2. The voltage on winding S3 is half-wave rectified by diode CR21 and filtered by capacitors C12 and C18. This unregulated voltage, -17 V, is applied to the case connection (case) of a linear regulator, ML5 which is a self-contained three terminal integrated circuit located on a common heat sink with ML4 and ML6, but electrically isolated from the heat sink.

Capacitors C29 and C34 are connected as close as possible to the input (case) and the output (2) of the regulator to filter high frequency load transients. Note the ground polarity connection of C18 and C34.

4. +42 V Supply

The +42 V supply is derived from a separate secondary winding of T2. The voltage on winding S4 is half-wave rectified by diode CR20 and filtered by capacitors C17 and C19.

Resistor R16 establishes the minimum load for the +42 V output.

The 1.0A slow blow fuse prevents printer head damage, if a printer head driver transistor shorts on the logic board.

The LED indicator (CR31) is "ON" whenever the +5 V output is present. Resistor R28 limits the current through the diode.

Additional filtering of the +42 V output is provided by a 1500uf or 2400uf capacitor on the logic board.

5. Voltage Sense

Feedback to the input of the error amplifier of the pulse width modulator is provided by a precision resistor divider consisting of R26 and R23. This voltage is fed through R24 to the negative error input of the pulse width modulator, and is then compared to the V_{REF} voltage at the positive error input.

An internally derived correction voltage adjusts the pulse width of the output signal, such that the compared voltage difference is minimum.

430770 POWER SUPPLY 410701 CIRCUIT CARD

1. Operation

The ac line voltage is directly converted to dc by a bridge rectifier connected directly to the ac input and filtered by a capacitor on the output side of the bridge rectifier. The dc output is connected to a switching regulator which provides a regulated output of a nominal 90 V. This output is connected to a doubleended inverter transformer which provides line isolation and transformer power to three low voltage secondary circuits where rectification is performed.

The +5 V, +12 V and -12 V outputs are derived from three separate windings which drive integrated circuit voltage regulators. These regulators are of the linear type.

The protective ground is not connected to the primary circuit ground. Care must be exercised during troubleshooting to prevent direct connection of these grounds because this will effectively bypass one of the bridge rectifier diodes and cause full line voltage to be directly applied to another diode in the forward direction. This rectifier and other line components will fail under this condition.

The secondary voltage returns are tied together and directly connected to the protective ground. However, isolation is maintained between the ac line and the secondary circuits.

430770 POWER SUPPLY 410701 CIRCUIT CARD (Contd)

2. AC Line Rectifier

The ac to dc rectification occurs through the full-wave bridge consisting of the four diodes CR1, CR2, CR3 and CR4 (B5). Capacitor C1 filters the dc.

The anodes of CR1 and CR2 and the negative end of C1 are connected to a common bus for all primary circuits. This bus is not to be confused or connected with any ground bus on the secondary circuits unless the power supply is floated through an isolation transformer. Grounding of the primary bus might cause destruction of diode CR1, as well as thermistor RT1.

3. Start Circuits

Upon initial application of ac power, capacitor C1 charges to peak line voltage. Resistor R1 (B6), supplies bias current through steering diode CR25 (C7), to the base of the switcher driver transistor Q5. The emitter of Q5 is connected through diode CR23 to the control voltage bus and Q5 remains "ON" until the control voltage becomes greater than 20 V which is determined by zener diode CR32 (C6).

When Q5 is "ON" the main switcher transistor, Q1 (B6), is "ON" and supplies current from C1 to charge the switching regulator output capacitor C2 (B8). The output capacitor is connected to the inverter transformer center-tap and also to the control voltage bus through current limiting resistor R6 (C9).

The switching regulator and inverter transformer drive control functions are performed by integrated circuit ML1 (F9). This circuit requires about 12 mA. The inverter drive base current is supplied by the control bus and limited to about 50 mA by resistor R19 and R20 (D8).

During start-up, the inverter base drive is inhibited by grounding (Pin 9) of ML1 through diode CR26 (E11), and R36. When the control bus voltage reaches 15 V, zener diode CR33 (C11), starts to conduct which removes the inhibit signal from (Pin 9) and enables ML1 to begin generating drive pulses at a low duty cycle.

To keep power loss to a minimum, the control bus voltage supply resistor R6, supplies about 20 mA. This is not sufficient to supply ML1 and full inverter drive transistor base currents. Therefore the control bus voltage will rise only to a point necessary to give about 20 percent duty cycle base drive pulses as controlled by zener diode CR33. However, when these pulses are generated, the voltage induced in transformer T1 feedback winding is applied to the control voltage bus through full-wave rectifier diodes CR12 (J10), and CR46 to raise the control voltage immediately to about 25 V. This removes the ML1 (Pin 9) inhibit signal and enables ML1 to operate in the full control mode.

4. Switching Regulator

The switching regulator section contains the switching transistor Q1 (B6), catch diode CR5, inductor L1, and capacitor C2. Control of the regulator is performed by integrated circuit ML1 which contains the oscillator, voltage reference, error amplifier, pulse width modulator, pulse steering flip-flop, dual alternating output switches, current limiting and shutdown circuitry. The oscillator is set at a nominal 35 KHz, controlled by C14 and R31 (F9).

The switcher transistor, Q1, is driven by a current amplifier, Q4, and a constant current configured transistor, Q5, which is turned on and off by ML1. Since Q5 is connected to both output switches of ML1 through diodes CR30 and CR31 (D8), the main switching transistor, Q1, is turned on each time either inverter driver transistor is turned on.

The output of the switching regulator section is connected to inverter transformer T1. Feedback voltage is supplied by the T1 feedback winding, (Pins 4, 5 and 6) and is full-wave rectified by diodes CR12 and CR46 (J10), filtered by capacitor C4, and connected to the inverting input of the ML1 error amplifier, (Pin 1) through the voltage divider R30 and R28 (E10). The reference voltage, (Pin 16) of ML1, is divided by resistors R27 and R29 and applied to the noninverting input of the ML1 error amplifier, (Pin 2).

During normal operation, the start-up function of Q5 is inhibited by the reverse bias on diode CR25 (C7).

5. Inverter Drive Circuit

Power is transferred from the primary to the secondary circuits through the inverter transformer, T1. The transformer primary is double ended, bifilar wound with the center tap connected to the output of the switching regulator. In normal operation the center tap voltage is a nominal 90 Vdc.

Each side of the transformer primary is alternately switched to ground by transistors Q2 and Q3. These transistors are driven by the switch outputs of integrated circuit ML1 through diodes CR40 (H10), and CR41 (I10). Base current to Q2 and Q3 is controlled by resistors R19 and R20 (D8), respectively. The inverter drive frequency is one-half of the switching regulator frequency. The base drive pulse duty cycle supplied by ML1 varies in the same proportion as the switching regulator drive duty cycle to compensate for variation in line voltage, ripple and load.

To prevent inverter drive duty cycle fold back and to supply additional base current, the feedback winding of T1 is connected to the bases of Q2 and Q3 through resistor diode networks R17 (J12), CR42 and R18, CR43 respectively. This arrangement supplies about 50 mA of base current to the conducting drive transistor.

Inverter drive transistor turnoff for Q2 and Q3 is performed by transistors Q6 and Q8 (H10) respectively. These commutating transistors shunt the feedback base drive to ground and remove the stored charge from the inverter drive transistors. Q6 and Q8 are driven by the switch outputs of ML1 through R-C networks, R26 (E8), C19 and R49, C20 respectively. They are alternately turned on when the respective output of ML1 removes base drive to the particular inverter drive transistor, Q2 or Q3. They will remain on for 3 to 5 microseconds, which is sufficient to insure that the transformer T1 has switched state.

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B. CIRCUIT DESCRIPTIONS (Contd)

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LOGIC VOLTAGES

1. +5 V Supply

The +5 V supply is derived fron a secondary winding of T1. The voltage on winding S1 is full-wave rectified by diodes CR13 and CR14 (H13), and filtered by capacitors C8 and C26. This semiregulated voltage, +8.5, is applied to the input of a linear regulator, ML5, which is a self-contained three terminal integrated circuit located on a common heat sink with ML3 and ML4. Capacitors C9 and C21 on the output of the regulator filters high frequency load transients.

2. +12 V Supply

The +12 V supply is derived from a secondary winding of T1. The voltage on winding S2 is half-wave rectified by diode CR16 (F13), and filtered by capacitors C6 and C27. This semiregulated voltage, +15 V, is applied to the input of a linear regulator, ML3, which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML4. Capacitors C10, C22 and C23 on the output of the regulator filter high frequency load transients.

3. -12 V Supply

The -12 V supply is derived from a secondary winding of T1. The voltage on winding S3 is half-wave rectified by diode CR15 (G13), and filtered by capacitors C7 and C28. This semiregulated voltage, -15 V, is applied to the input connection of a linear regulator, ML4, which is a self-contained three terminal integrated circuit located on a common heat sink with ML5 and ML3. Capacitors C11, C24 and C25 on the output of the regulator, filter high frequency load transients.

FAULT PROTECTION ON SECONDARY

1. Short Circuit Protection

The +5 V, +12 V and -12 V supply out puts are protected against short circuits to ground by means of the current limiting characteristics inherent in the integrated circuit voltage regulator which is in each of these outputs. The +5 V fault current is limited to approximately 4 amperes, the +12 V and -12 V fault currents are limited to approximately 1.5 amperes. Whenever the fault is removed, the output voltage automatically recovers.

These regulators are also thermally protected so that in the event that their power dissipation in conjunction with the ambient temperature exceeds their limit, automatic shutdown occurs. Whenever the internal temperature decreases to a safe level, the device will reset and restore the output voltage.

2. Output Regulator Protection Circuits

Diodes CR17, CR20 and CR21, placed across the input/output terminals of output linear regulators, ML5, ML3 and ML4 respectively, protect the linear regulators from potential reverse bias conditions when an overvoltage shutdown condition occurs.

Diodes CR18, CR19 and CR22, placed from output to ground on the output terminals of linear regulators ML5, ML3 and ML4 respectively, protect the linear regulators from a load connected from an output to a voltage of an opposite polarity.

3. Overvoltage Protection

Each secondary output voltage has an overvoltage sense circuit which will cause the power supply to shut down whenever an overvoltage is detected on an output.

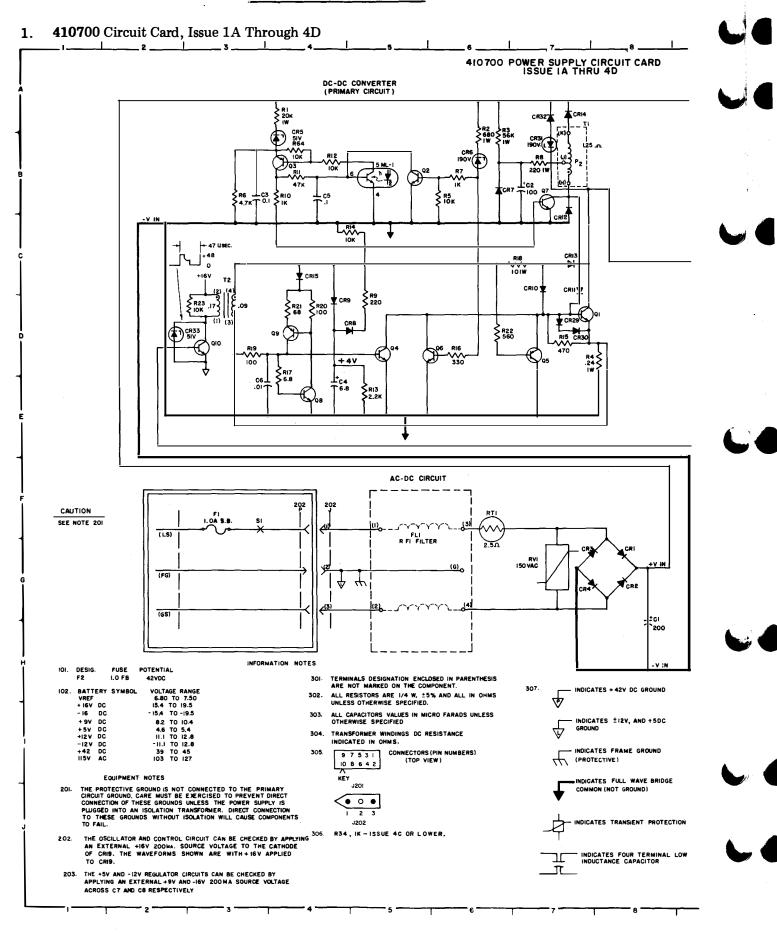
Zener diode CR35 (H16), connected to the +5 V supply and zener diode CR36 (D16), connected to the +12 V supply are diode coupled by CR28 and CR29 to the base of transistor Q9. Resistor R44 limits the current through the photo-diode. An overvoltage condition on either the +5 V or +12 V supplies will break down the corresponding zener diode, thus supplying base current to the transistor Q9 causing the photo-diode to conduct.

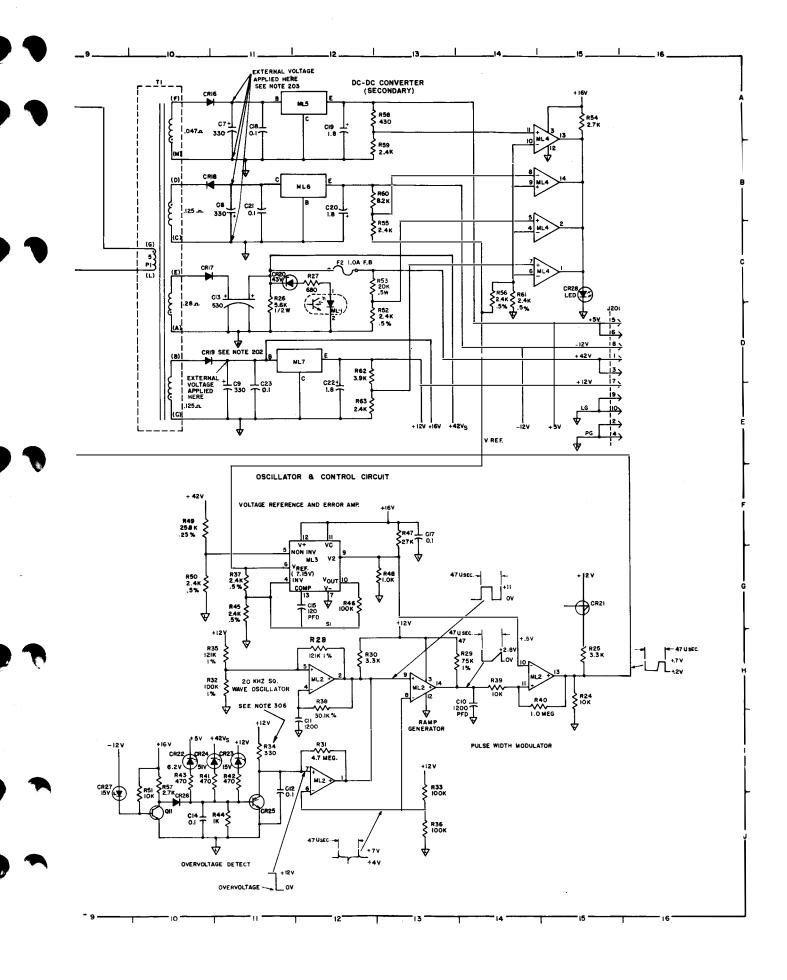
Zener diode CR37 (G16), connected to the -12 V supply, is diode coupled by CR27 to the cathode of the Q10 (E16) transistor. Resistor R52 limits the base current through the base of Q10. An overvoltage condition on the -12 V qupply will break down the zener diode, thus supplying current to transistor Q10, which will turn on the photodiode in ML2.

The associated ML2 phototransistor will turn "ON" when the ML2 photo-diode conducts. Transistor Q7 (C11) turns "ON" when the phototransistor turns "ON" and the resulting latch maintains a bias on ML1 shutdown (Pin 10). Commutation transistors Q6 (H10) and Q8 are also turned "ON". This action inhibits operation of the switching regulator and inverter drive circuits. The semiregulated secondary voltages from T1 are removed. In order for the supply to recover, the input line voltage must be removed for approximately 20 to 30 seconds.

Zener diode CR47 (E11) and transistor Q7 forms a overvoltage protection circuit on the feedback voltage. If transistor Q1 shorts or turns full-on, the full input voltage (140 Vdc) will be applied to the dc-dc converter resulting in higher secondary voltages. To prevent excess heat or damage to components, zener diode CR47 will sense the rise in voltage, transistor Q7 will turn-on, causing the dc-dc connector to latch off. Zener diode CR34 (C20) in conjunction with CR33, limit the voltage applied to ML1 during overvoltage conditions.

C. CIRCUIT DIAGRAMS





410700 Circuit Card, Issue 5A Through 8B

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C. CIRCUIT DIAGRAMS (Contd)

410700 POWER SUPPLY CIRCUIT CARD ISSUE 5A THROUGH 8B DC-DC CONVERTER (PRIMARY CIRCUIT) ₹ R1 20K 1W L_ __ _] TP = 1 CRIA CR32 R3 564 CR31 3 RB \mathcal{D}_{as} 220 1 - ANA C2 (04) C5 CRIS SEE NOTE 310 ÷ - 47 U SEC 48 <u>`</u>`L';; RIB 10.1 +16V CRIS т2 TP-3 CRIO сви¥ \$ 220 T CR9 R23 .17 .09 ₹R20 CR2 (1) (3 CRB IP=4 **₹**822 560 99 SEE NOTI 08 RI 6 R R4 24 1W CR33 100 **≶**817 ≶6.8 (r . ₽ ₽ ₽ .01 010 **₹**813 2.2K TP-2 AC-DC CIRCUIT 202 202 CAUTION S.B SEE NOTE 201 ¢ \sim (LS) FLI R FI FILTER 2.5.0 RVI 150 VAC (G) (FG) 4 ♦ C.R.2 <u>/(3</u>) (GS) SEE NOTE 309 LCI6 INFORMATION NOTES FUSE POTENTIAL IOI. DESIG. F2 42VDC 30 TERMINALS DESIGNATION ENCLOSED IN PARENTHESIS ARE NOT MARKED ON THE COMPONENT. 102. BATTERY SYMBOL WREF + 16V DC - 16 DC + 9V DC + 5V DC + 12V DC - 12V DC + 42 DC 115V AC VOLTAGE RANGE 6.80 TO 7.50 15.4 TO 19.5 15.4 TO 19.5 8.2 TO 10.4 4.6 TO 5.4 11.3 TO 12.6 -11.1 TO 12.8 39 TO 45 306 - INDICATES +42V DC GROUND ALL RESISTORS ARE 1/4 W, ±5% AND ALL IN OHMS UNLESS OTHERWISE SPECIFIED 302. 4 303. ALL CAPACITORS VALUES IN MICRO FARADS UNLESS OTHERWISE SPECIFIED INDICATES \$12V, AND +5 DC GROUND TRANSFORMER WINDINGS DC RESISTANCE INDICATED IN OHMS. 304 INDICATES FRAME GROUND 39 TO 45 103 TO 127 305 CONF NECTORS (PIN NUMBERS) (TOP VIEW) 97531 Ψ. (PROTECTIVE) 10 8 6 4 2 EQUIPMENT NOTES KEY INDIGATES FULL WAVE BRIDGE COMMON (NOT GROUND) 201. THE PROTECTIVE GROUND IS NOT CONNECTED TO THE PRIMARY CIRCUIT GROUND. CARE MUST BE EXERCISED TO PREVENT DIRECT CONNECTION OF THESE GROUNDS UNLESS THE POWER SUPPLY IS PULIGED INTO AN ISOLATION TRANSFORMER. DIRECT COMMECTION TO THESE GROUNDS WITHOUT ISOLATION WILL CAUSE COMPONENTS TO THESE GROUNDS WITHOUT ISOLATION WILL CAUSE COMPONENTS TO THESE. J201 . . . 23 INDICATES TRANSIENT PROTECTION J202

INDIGATES FOUR TERMINAL LOW INDUCTANCE CAPACITOR

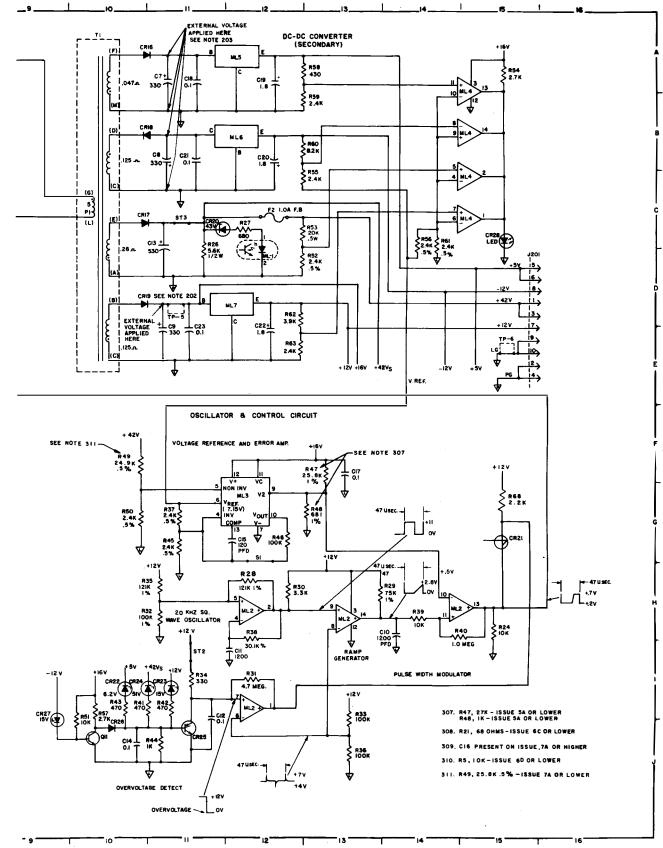
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203. THE +5V AND -12 V REGULATOR CIRCUITS CAN BE CHECKED BY APPLYING AN EXTERNAL + 9V AND -16V 200 MA SOURCE VOLTAGE ACROSS C7 AND C8 RESPECTIVELY

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THE OSCILLATOR AND CONTROL CIRCUIT CAN BE CHECKED BY APPLYING An External +164 200MA. Source voltage to the cathode of Crib. The waveforms shown are with +164 applied to Crib.

202.



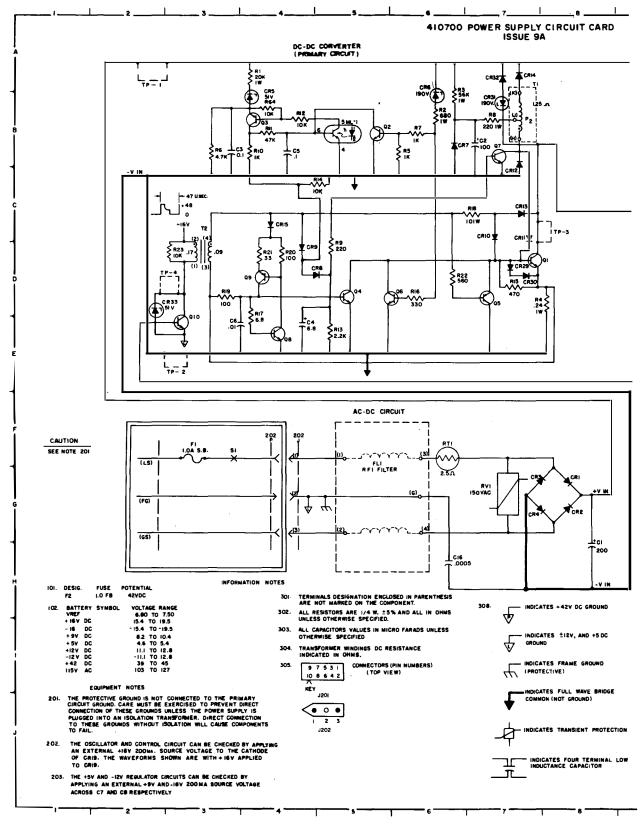
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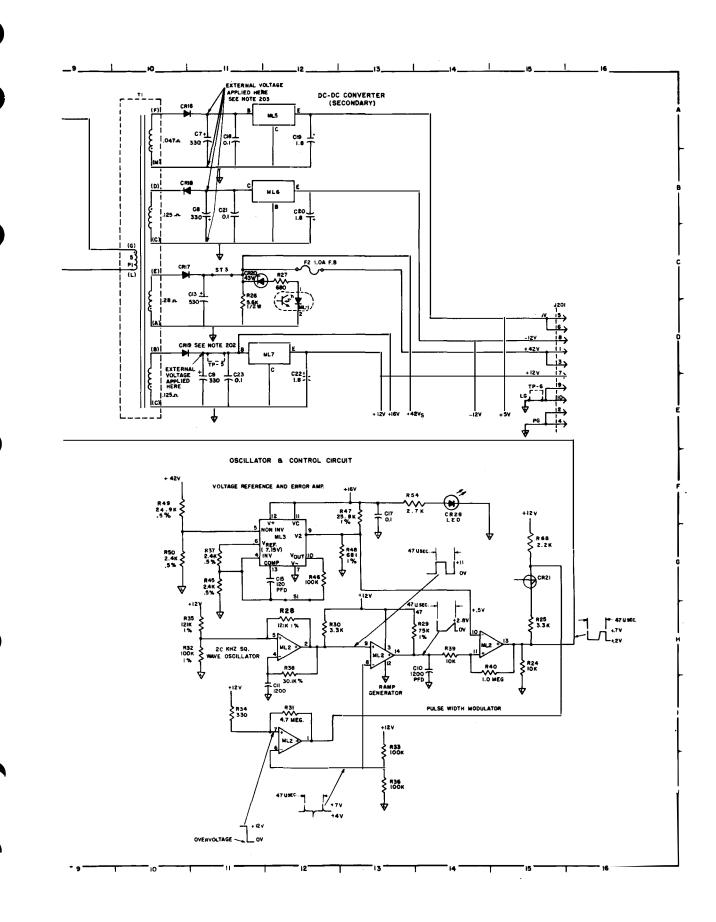
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C. CIRCUIT DIAGRAMS (Contd)

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3. 410700 Circuit Card, Issue 9A



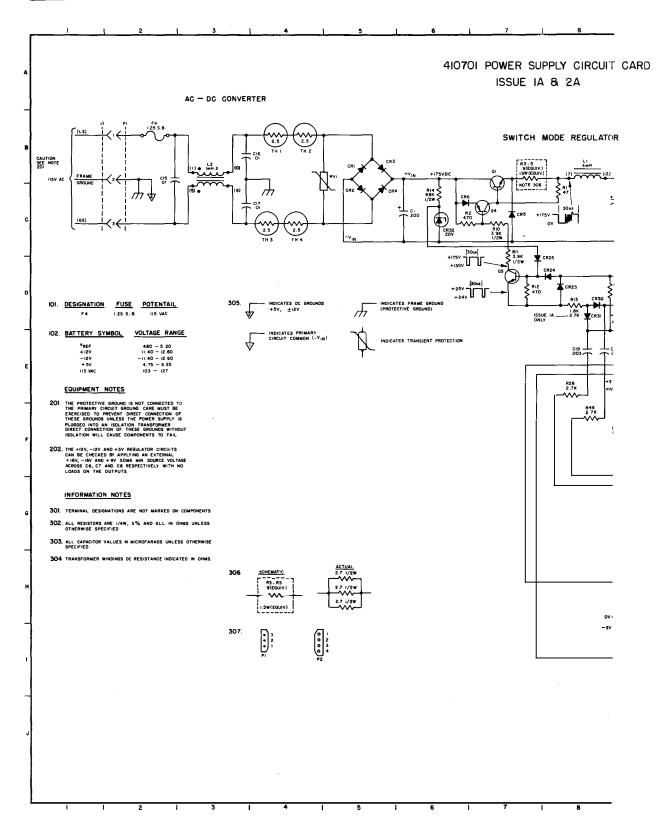


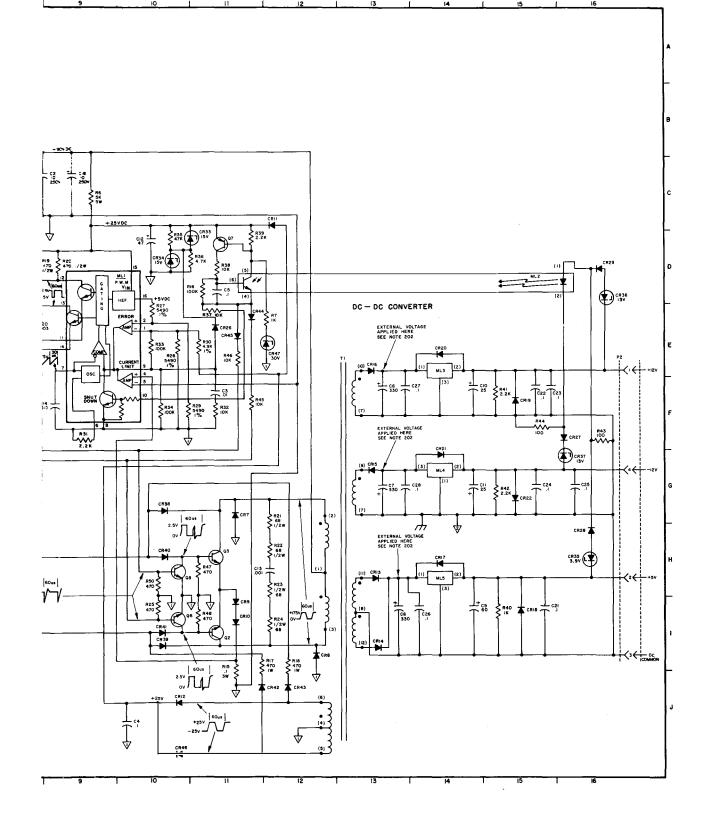
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C. CIRCUIT DIAGRAMS (Contd)

4. 410701 Circuit Card, Issues 1A and 2A

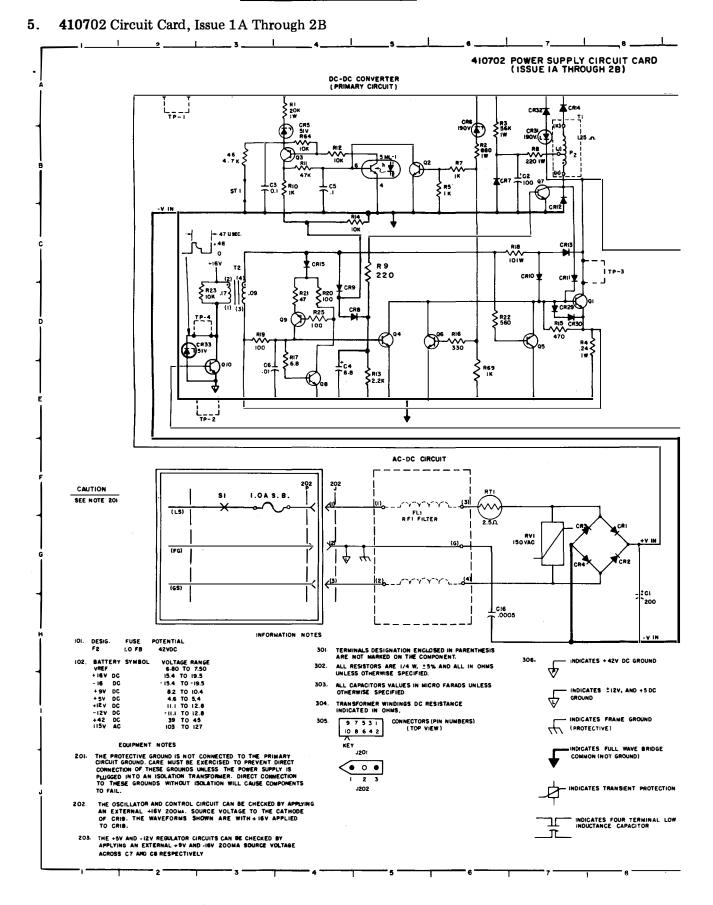


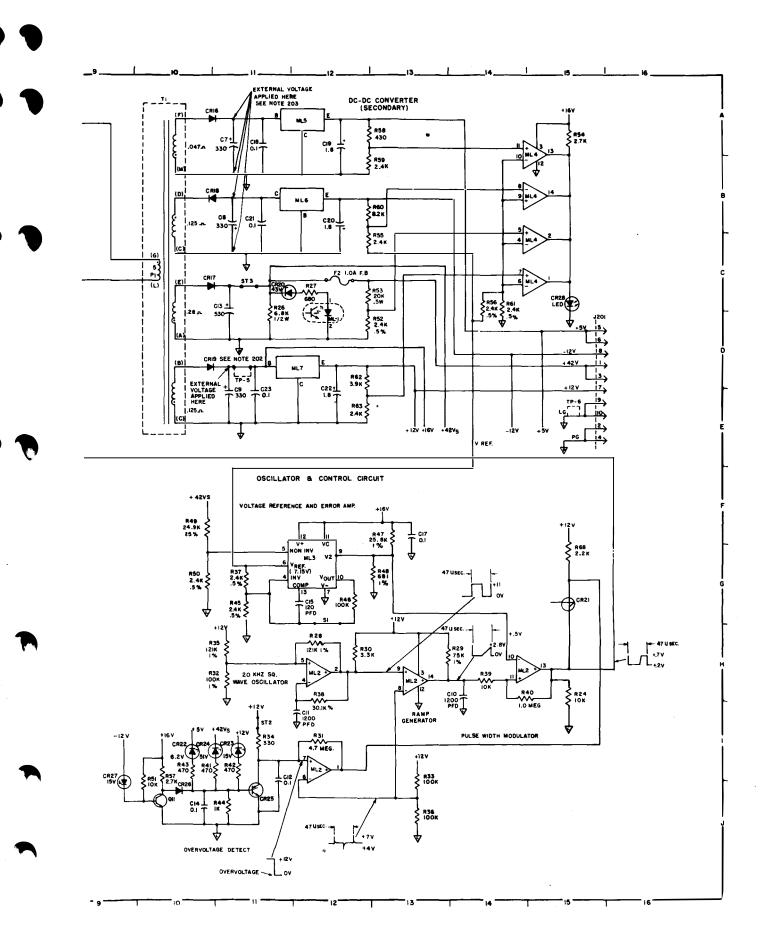


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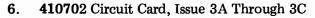
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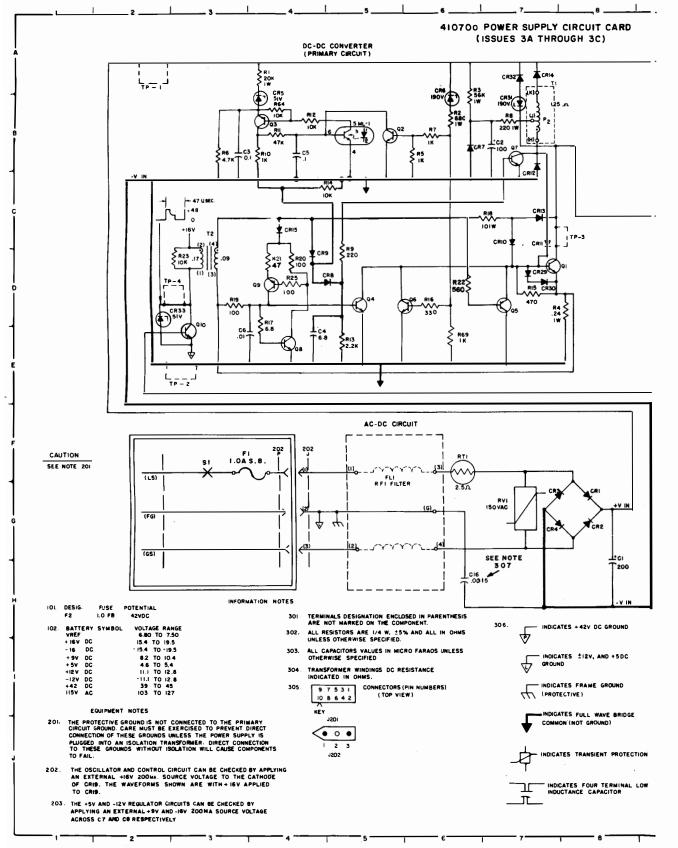
C. CIRCUIT DIAGRAMS (Contd)

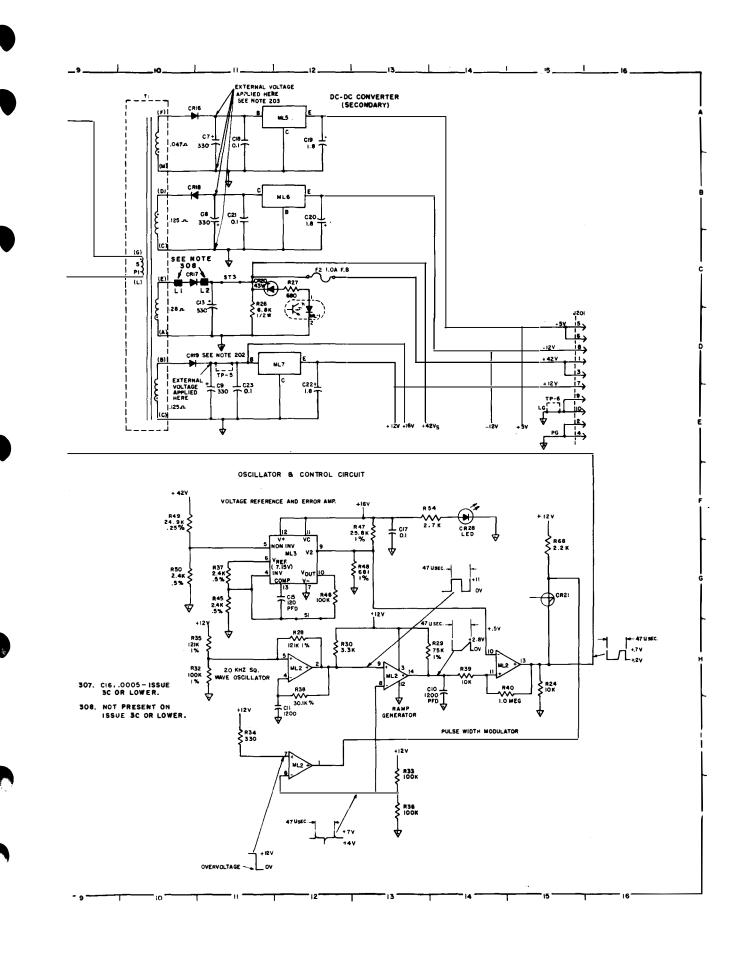




C. CIRCUIT DIAGRAMS (Contd)



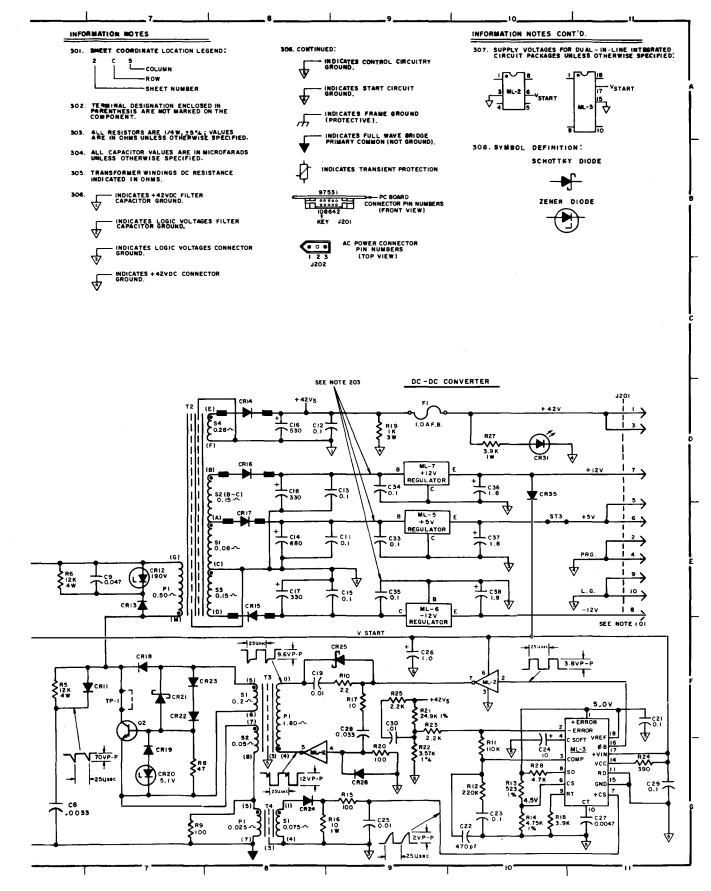




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C. CIRCUIT DIAGRAMS (Contd)

7. 410703 Circuit Card, Issue 1A 2 EQUIPMENT NOTES DRCUIT NOTES 410703 POWER SUPPLY 201. THE PROTECTIVE EROUND IS NOT CONNECTED TO TH PRIMARY CIRCUIT COMMON. CARE MUST BE EXERCIS TO PREVENT DIRECT COMMECTION OF THESE POINT UNLESS THE POTER SUPPLY IS PLUGGED INTO AN ISOLES POINTS WITHOUT THE USE OF MUSICATION TRANSFORMER WILL CAUSE COMPONENTS TO FAIL 101. VOLTAGE SYMBOL AND RANGE: VOLTAUL SYMBOL VREF DC VSTART DC +42VS DC JL AND RANGE: VOLTAGE RANGE 4.95 11.4 70 20.6 27.5 70 375 WOLTAGE CIRCUIT CARD (ISSUE IA) THE PULSE WIDTH MODULATOR ML-3 CAN BE CHECKED BY APPLYING AN EXTERNAL +12 VDC 200 MA SOURCE VOLTAGE TO THE CATHODE OF CR6 WITH NO AC POWER APPLIED. 202. DC DC DC DC DC PRIMARY COMMON -VIN +42V +12V +5V -12V 38.6 TO 42.0 11.4 TO (2.6 4.75 TO 5.25 -11.4 TO -12.6 THE +5V,+12V AND-12V REGULATOR CIRCUITS CAN BE CHECKED BY APPLYING AN EXTERNAL + 9VDC,+16VDC AND-16VDC 200MA. SOURCE VOLTAGE ACROSS C33, C34 AND C35 RESPECTIVELY. 203. 115V 230V AC 103 TO 127 195 TO 265 102. STRAP NOTES: WITH ST-2 IN THE 230V POSITION, THE FUSE FI SHALL BE A 1.0A SLOW BLOW. ON THE CIRCUIT BOARD PROVISIONS HAVE BEEN MADE TO MOVE THE ST-2 STRAP TO THE 115V POSITION, THE FUSE FI SHALL THEN BE A 1.5A SLOW BLOW. AC-DC CIRCUIT (SEE NOTE 102) • 1 15 v J 202 `<" RT2 SI RO [3] -0 0 (LS) €⁽²⁾ ï FLI SEE NOTE 1021 _;;; _;;; CAUTION SEE NOTE 201 297,VDC 1 Ì. (PG) <u>;</u> +VIN (3) RVI 275VAC <u>|_0</u> (4) (GS) C4 390 十覧 48VDC + ₹ 84 39K 2W 十 。 C5 390 1 - V IN (3) (5) 17.9 VDC IIVDC ML-1 +5V REGULATOR CRE 0 \$ R2 270 SEE NOTE 202 <u>+</u> C2 C3 C I 1000 \$ RI 270 1/2W (SEE NOTE 306)



CIRCUIT DIAGRAMS (Contd) С. 8. 410704 Circuit Card, Issue 1A 2 CIRCUIT NOTES EQUIPMENT NOTES 410704 POWER SUPPLY THE PROTECTIVE GROUND IS NOT COMMECTED TO THE PRIMARY CIRCUIT COMMON. CARE MUST BE CLERCOME TO PREVENT DIRECT CONNECTION OF THEE POINTS. UNLESS THE POWER SUPPLY IS PLORED MITD AN INTERE POINTS WITHOUT THE USE OF AN ISOLATOM TRANSFORMER WILL CAUSE COMPONENTS TO FAIL. IOI. VOLTAGE SYMBOL AND RANGE :
 SOL AND RANGE.

 VOLTAGE RANGE.

 4.95 TO 5.05

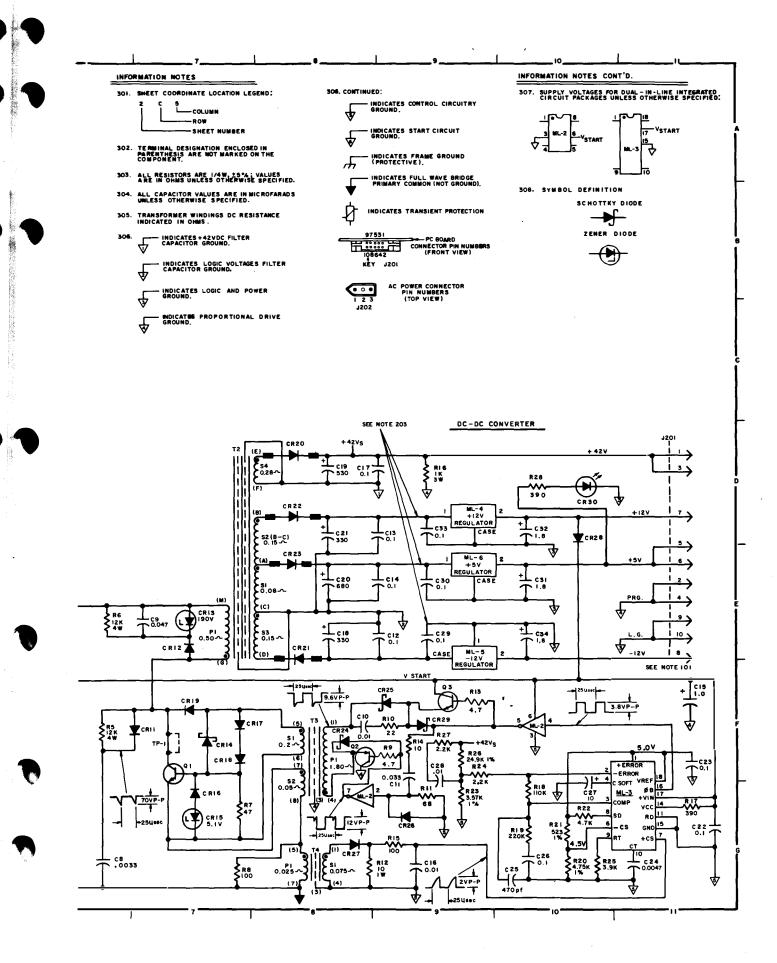
 11.4 TO 12.6

 36.6 TO 42.0

 275 TO 375 WITH RESPECT TO PRIMARY COMMON
 201. CIRCUIT CARD SYMBOL (ISSUE IA) VREF VSTART +42Vs +VIN DC DC DC DC THE PULSE WIDTH MODULATOR ML-3 CAN BE OWNED BY APPLYING AN EXTERNAL +12 VOC 200MA SOURCE VOLTAGE TO THE CATHODE OF CR6 WITH NO AC POWER APPLIED. 202. PRIMARY COMMON 38.6 TO 42.0 11.4 TO 12.6 4.75 TO 5.25 -11.4 TO -12.6 DC DC DC DC DC -VIN +42V + 12 V + 5V - 12 V THE +5V, +12V AND -12V REGULATOR CIRCUITS CAN BE CHECKED BY APPLYING AN EXTERNAL +9VDC, +16VDC AND -16VDC 200MA.SOURCE VOLTAGE ACROSS C30, C33 AND C29 RESPECTIVELY. 203. 115V 230V AC AC 103 TO 127 195 TO 265 102. OPTION SWITCH NOTES: WITH S2 IN THE 230V POSITION, THE FUSE FI SHALL BE A 1.0 A SLOW BLOW. WITH S2 IN THE 115V POSITION, THE FUSE FI SHALL BE 1.5A SLOW BLOW. AC-DC CIRCUIT (SEE NOTE 102) 115 V S 2 P202 J 2 0 2 C RT2 €^m ក្រា (i) 0 o LS FLI Ĺ (6) -0 CAUTION SEE NOTE 201 230 V 297,VDC (2) **,** (PG) +VIN ١ I <u>(3)</u> RVI 275VAC <u>__</u> (4) (GS) ₹ 83 59K 2W C7 390 十続 48VDC ₹ 84 39K 2W 上て - C6 • 390 C5 0.01 -v., (3 (5) IIVDC 17.9 VDC ML-1 +5V REGULATOR \$R2 SEE NOTE 202 C 2 1.8 C 3 CI 0.1 $\overline{\mathbf{T}}$ $\overline{\tau}$ T \$ RI 270 1/2 W \mathbf{r} (SEE NOTE 306)

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MANUAL 523, 4-39



PART 5 - PARTS

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A. GENERAL

Parts, identification and numbering information for the 430700, 430760, 430770 and 430780 power supply assemblies is provided in this part.

All replaceable parts are included. Examples of nonreplaceable parts not shown but included in higher order assemblies are as follows:

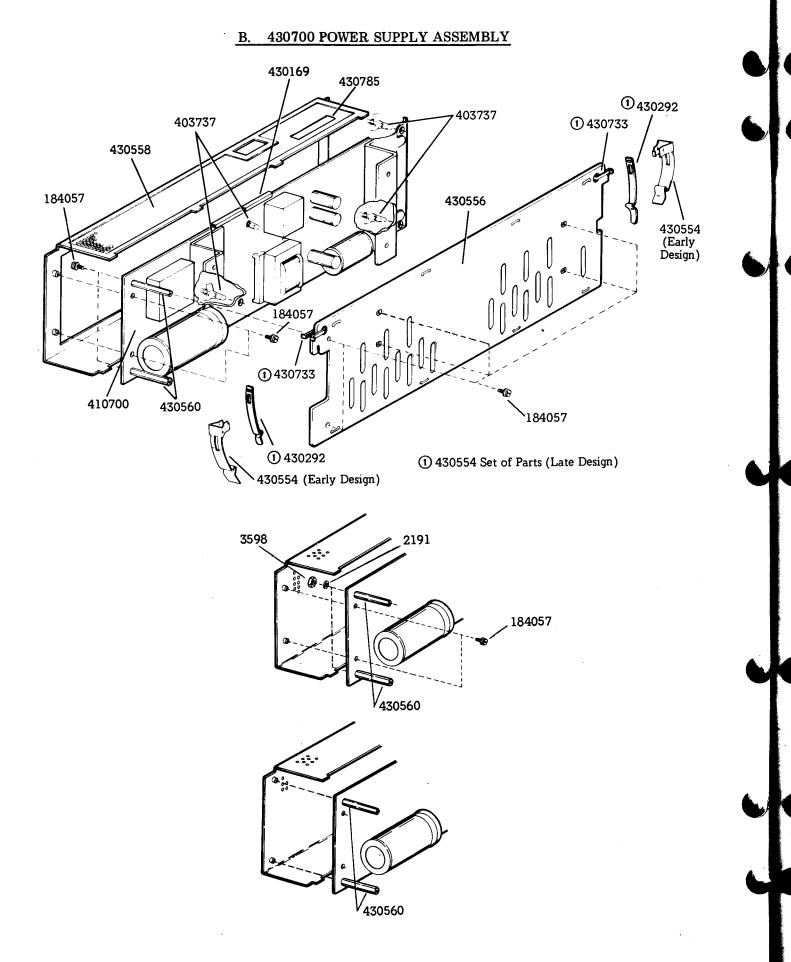
- 1. Part as supplied would not fit if installed.
- 2. May require manufacturing or shop methods not provided in this manual.
- 3. Part of crimped, riveted, pressed or welded assembly.
- 4. Serial number or registration plates.

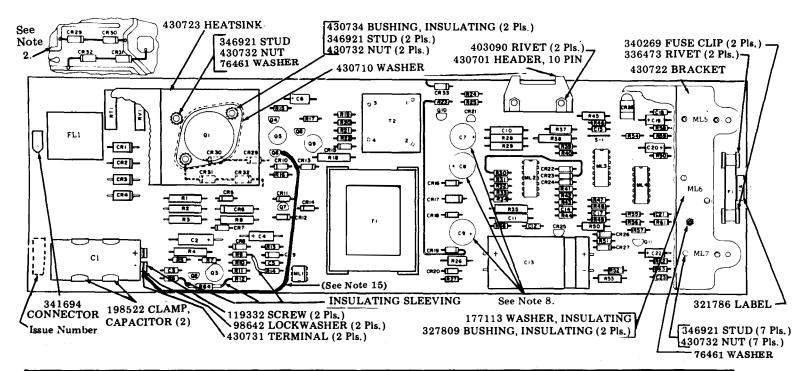
Parts are listed in the index in numerical order and indicate the page on which the parts appear.

When ordering replaceable components, unless otherwise specified, prefix each part number with the letters "TP" (ie, 430019).

Troubleshooting and disassembly/reassembly information for these parts is provided in PARTS 2 an 3, respectively.

When disassembly/reassembly information is not shown, the illustrations in this part provide sufficient information.





REF. DESIG.	PART NO. REQ.	NOTE	DESCRIPTION	REF. DESIG.	PART NO. REQ.	NOTE	DESCRIPTION	REF. DESIG.	PART NO. REQ.	NOTE	DESCRIPTION
C1	430706		CAPACITOR, 200 MFD	CR1	408037		DIODE, 400 V	CR24	430725		DIODE, ZENER 51 V
C2	310930		CAPACITOR, 100 MFD	CR2	408037		DIODE, 400 V	CR25	336694		THYRISTOR, SCR 8A
C3	405324		CAPACITOR, .1 MFD	CR3	408037		DIODE, 400 V	CR26	197464		DIODE, 1N4148
C4	333727		CAPACITOR, 6.8 MFD	CR4	408037		DIODE, 400 V	CR27	430724		DIODE, ZENER 15 V
C5	405324		CAPACITOR, .1 MFD	CR5	430725		DIODE, ZENER 51 V	CR28	405029		LED. PCB MOUNTABLE
C6	300057		CAPACITOR, .01 MFD	CR6	430713		DIODE, ZENER 190 V	C'R29	4 <u>306</u> 05		DIODE, IN4936
C7	430704		CAPACITOR 330 MFD	CR7	430605		DIODE. 1N4936	CR30	430605		DIODÉ, IN4936
<u>C8</u>	430704		CAPACITOR, 330 MFD	CR8	300102		DIODE, 1N4156	CR31	430713		DIODE, ZENER 190 V
C9	430704		CAPACITOR, 330 MFD	CR9	430605		DIODE, 1N4936	CR32	430605		DIODE, IN4936
C10	430721		CAPACITOR, 1200 PFD	CR10	430605		DIODE, 1N4936	CR33	430725		DIODE, ZENER 51 V
C11	430721		CAPACITOR, 1200 PFD	CR11	430605		DIODE, 1N4936	FL1	430709		FILTER, RFI
C12	405324		CAPACITOR, .1 MFD	CR12	430605	1	DIODE, 1N4936	F2	120139	1	FUSE, IA
C13	430738		CAPACITOR, 530 MFD	CR13	430605		DIODE, 1N4936				
C14	405324		CAPACITOR, .1 MFD	CR14	430605		DIODE, 1N4936	ML1	335522	5	IC, OPTICAL COUPLER
C15	325034		CAPACITOR, 120 PFD	CR15	430605		DIODE, 1N4936	ML2	404239		QUAD VOLT COMPARATOR
				CR16	430605		DIODE, 1N4936	ML3	326823		REGULATOR, VOLTAGE
C17	405324		CAPACITOR, .1 MFD	CR17	430715	1	DIODE, 200 V 3A FR	ML4	404239	1]	QUAD VOLT COMPARATOR
C18	405324		CAPACITOR1 MFD	CR18	430605		DIODE. 1N4936	ML5	402202	1	REGULATOR, +5 V
C19	310929	2	CAPACITOR, 1.8 MFD	CR19	403752		DIODE, 1N4936	ML6	402204		REGULATOR, 12 V
C20	310929	2	CAPACITOR, 1.8 MFD	CR20	312401	3	DIODE, ZENER 1N4755A	ML7	402201		REGULATOR, +12 V
C21	405324		CAPACITOR 1 MFD	CR21	430729		DIODE, 4 LAYER			1 1	
C22	310929	2	CAPACITOR 1.8 MFD	CR22	321135		DIODE ZENER 1N4735A				
C23	405324		CAPACITOR, .1 MFD	CR23	430724		DIODE, ZENER 15 V				

REF. DESIG.	PART NO. REQ.	NOTE	DESCRIPTION	REF. DESIG.	PART NO. REQ.	NOTE	DESCRIPTION	REF. DESIG.	PART NO. REQ.	NOTE	DESCRIPTION
Q1	430711	15	TRANSISTOR, 450 V	R17	177101		RESISTOR, 6.8 1/2 W	R45	401067		RESISTOR, 2400.5%
Q2	400909		TRANSISTOR, 60 V NPN		178862		RESISTOR, 101 W	R46	321508		RESISTOR, 100 K 1/4 W
_Q3	325077		TRANSISTOR, 2N4355	R19	315948		RESISTOR, 100 1/4 W	R47	315988		RESISTOR. 27 K 1/4 W
Q4	400909		TRANSISTOR. 60 V NPN	R20	315948		RESISTOR. 100 1/4 W	I R48	321213		RESISTOR. 1 K 1/4 W
Q5	325077	l	TRANSISTOR, 2N4355	R21	335622		RESISTOR, 68 1/4 W	R49	430719		RESISTOR, 25.8 K .5%
Q6	400909		TRANSISTOR, 60 V NPN	R22	315951		RESISTOR, 560 1/4 W	R50	401067		RESISTOR, 2400.5%
Q7	400909		TRANSISTOR, 60 V NPN	R23	320275		RESISTOR, 10 K 1/4 W	R51	320275		RESISTOR, 10 K 1/4 W
Q8	400909	I	TRANSISTOR, 60 V NPN	R24	320275	2	RESISTOR, 10 K 1/4 W	R52	318803		RESISTOR, 2400 1/4 W
Q9	325077		TRANSISTOR, 2N4355	R25	315957		RESISTOR, 3300 1/4 W	R53	321258		RESISTOR, 20 K 1/2 W
Q10	400909		TRANSISTOR, 60 V NPN	R26	118186		RESISTOR, 5600 1/2 W	R54	315956		RESISTOR, 2700 1/4 W
Q11	400909		TRANSISTOR, 60 V NPN	R27	315971	3	RESISTOR, 680 1/4 W	R55	318803		RESISTOR, 2400 1/4 W
				R28	341596		RESISTOR, 121 K 1 %	R56	401067		RESISTOR, 2400.5%
R1	120211		RESISTOR 20 K 1 W	R29	341592		RESISTOR, 75 K 1%	R57	315956		RESISTOR, 2700 1/4 W
R2	182763	1	RESISTOR, 6801 W	R30	315957	1	RESISTOR, 3300 1/4 W	R58	336697		RESISTOR, 430 1/4 W
R3	118198	1	RESISTOR, 56 K 1 W	R31	327721	i	RESISTOR, 4.7 MEG. 1/4 W	R59	318803		RESISTOR, 2400 1/4 W
R4	430714		RESISTOR, .24 K 1 W	R32	324902		RESISTOR, 100 K 1%	R60	315961		RESISTOR, 8200 1/4 W
R5	320275		RESISTOR, 10 K 1/4 W	R33	321508		RESISTOR, 100 K 1/4 W	R61	401067		RESISTOR, 2400.5%
R6	315959		RESISTOR, 4700 1/4 W	R34	328785	7	RESISTOR, 330 1/4 W	R62	320026		RESISTOR, 3900 1/4 W
R7	321213	1	RESISTOR, 1 K 1/4 W	R35	341596	1	RESISTOR, 121 K 1%	R63	318803		RESISTOR, 2400 1/4 W
R8	144464	1	RESISTOR, 220 1 W	R36	321508		RESISTOR, 100 K 1/4 W	R64	320275	3	RESISTOR, 10 K 1/4 W
R9	318802		RESISTOR, 220 1/4 W	R37	401067		RESISTOR, 2400 .5%				
R10	321213		RESISTOR, 1 K 1/4 W	R38	324908		RESISTOR, 30.1 K 1%	RT1	430707		THERMISTOR
R11	318801	3	RESISTOR, 47 K 1/4 W	R39	320275		RESISTOR, 10 K 1/4 W	Γ			
R12	320275	1	RESISTOR, 10 K 1/4 W	R40	330641	1	RESISTOR, 1 MEG. 1/4 W	L			
R13	315955		RESISTOR, 2200 1/4 W	R41	320276	T T	RESISTOR , 470 1/4 W	RV1	430708		VARISTOR
R14	320275		RESISTOR, 10 K 1/4 W	R42	320276		RESISTOR, 470 1/4 W				
R15	320276		RESISTOR, 4701/4 W	R43	320276		RESISTOR, 470 1/4 W				
R16	328785	I	RESISTOR, 330 1/4 W	R44	321213	2	RESISTOR, 1 K 1/4 W	T1	430702		TRANSFORMER, POWER
		A	•		•			T2	430703		TRANSFORMER, PULSE
								1		1	

Note 1: Typical heat sink assembly.

Note 2: At customer identification Issue 2A, C19, C20, C22 was changed from 1 MFD, R23 was changed from 3.3K, R44 was changed from 10K, CR31, CR32 and CR33 were added.

Note 3: At customer identification Issue 3A, the following changes were made, CR20 was changed from 328696, R11 changed from 320275, R27 changed from 321213, R64 was added, and one lead of R14 was moved from ML-1 to base of Q7.

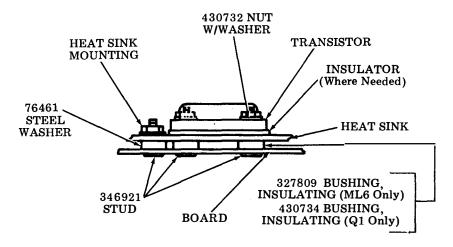
Note 4: At customer identification Issue 4A, conductor on noncomponent side from CR21 to R23 and pin 2 of 430703 transformer was cut at CR21. Conductor from R29 to C9 was cut on component side, strap added from left side of R23 to cathode of CR19 and strap added from left side of R30 to cathode of CR22. S1 replaced C16.

Note 5: At customer identification Issue 4B, ML1 was changed from 404325.

Note 6: At customer identification Issue 4C, the following change was made: bushing under Q1 changed from 327809 to 430734.

Note 7: At customer identification Issue 4D, R34 was changed from 321213.

See Note 1.



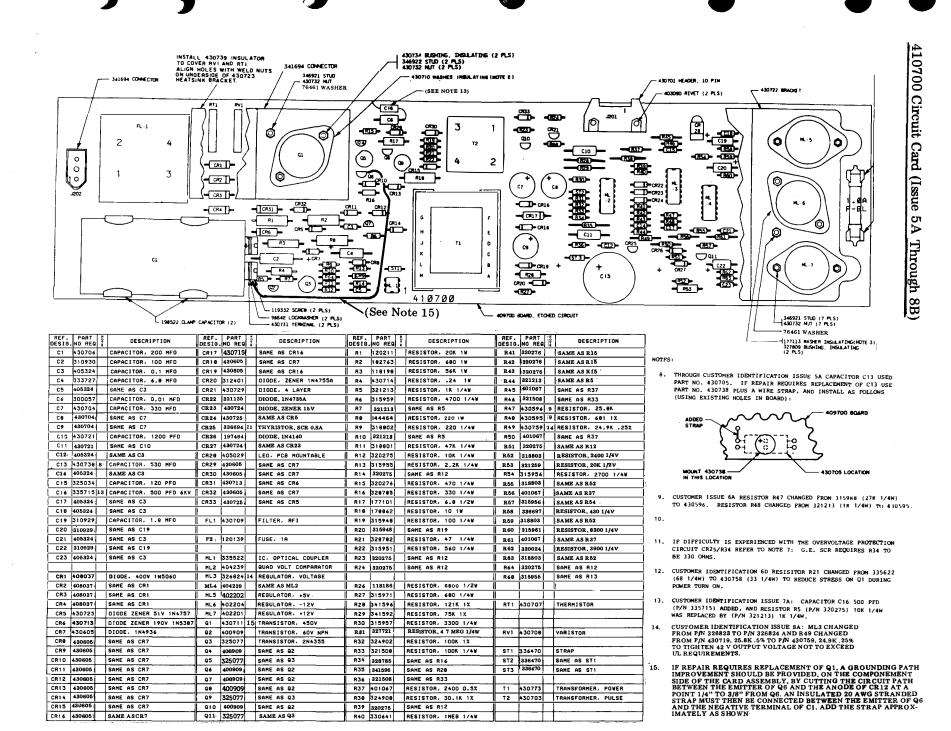
STRAP

336470

4

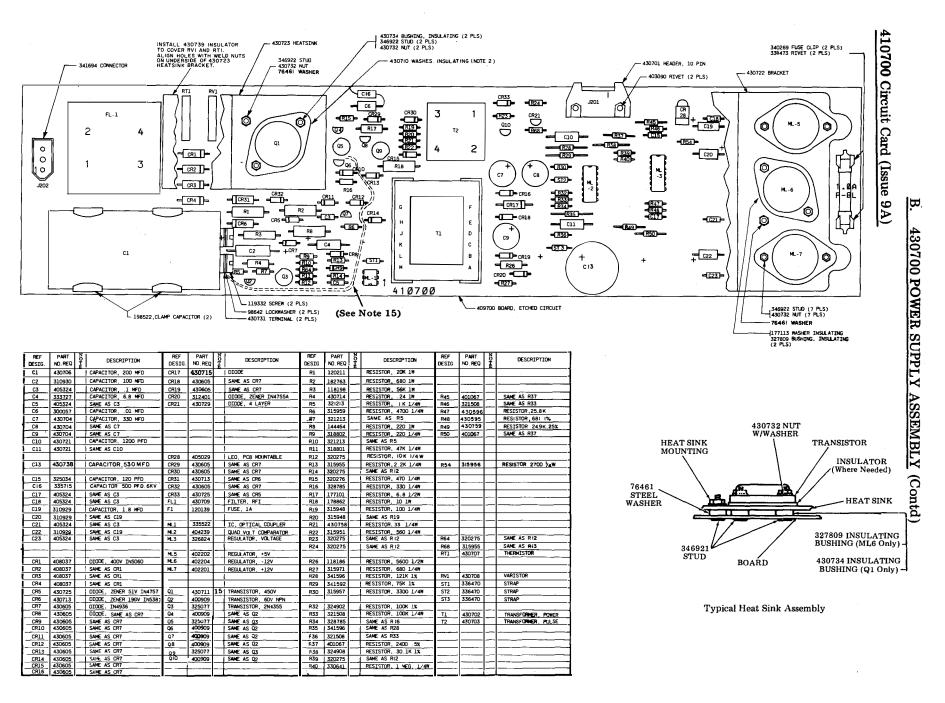
S1

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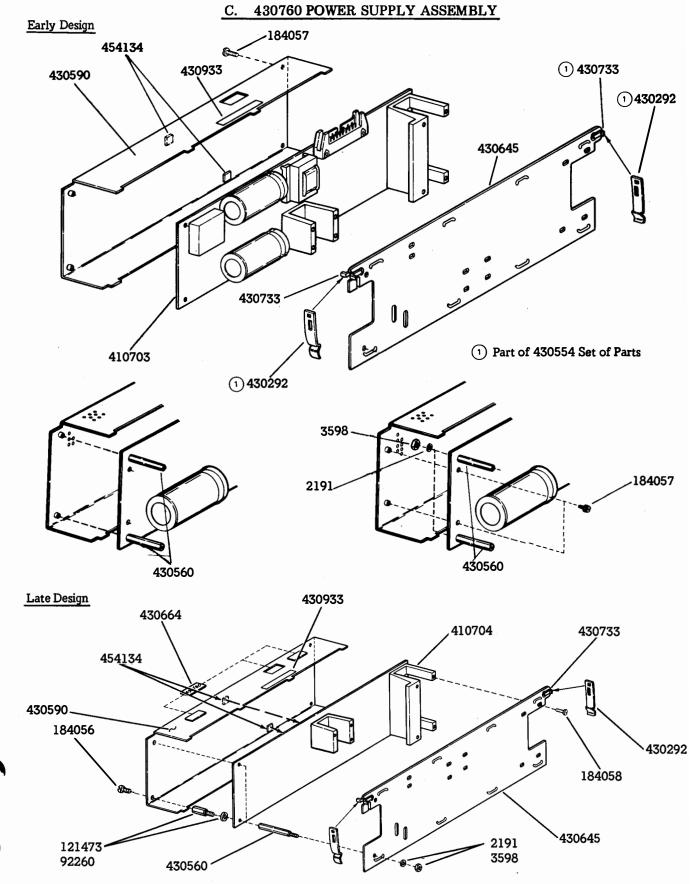


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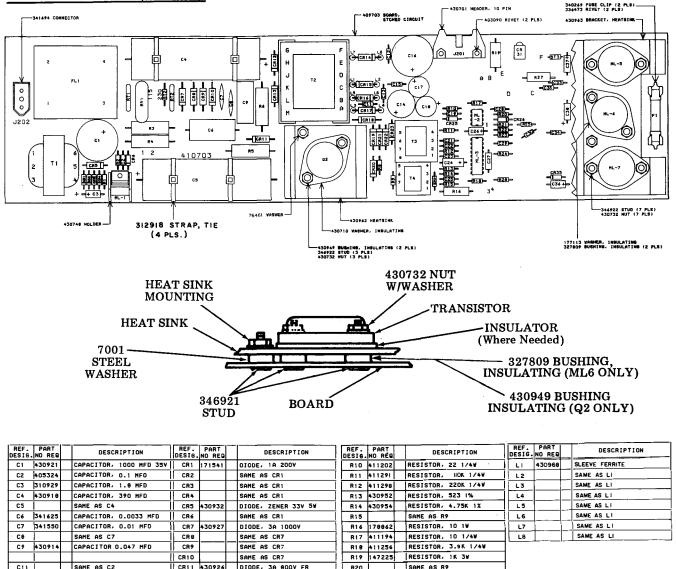
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523, 5-6

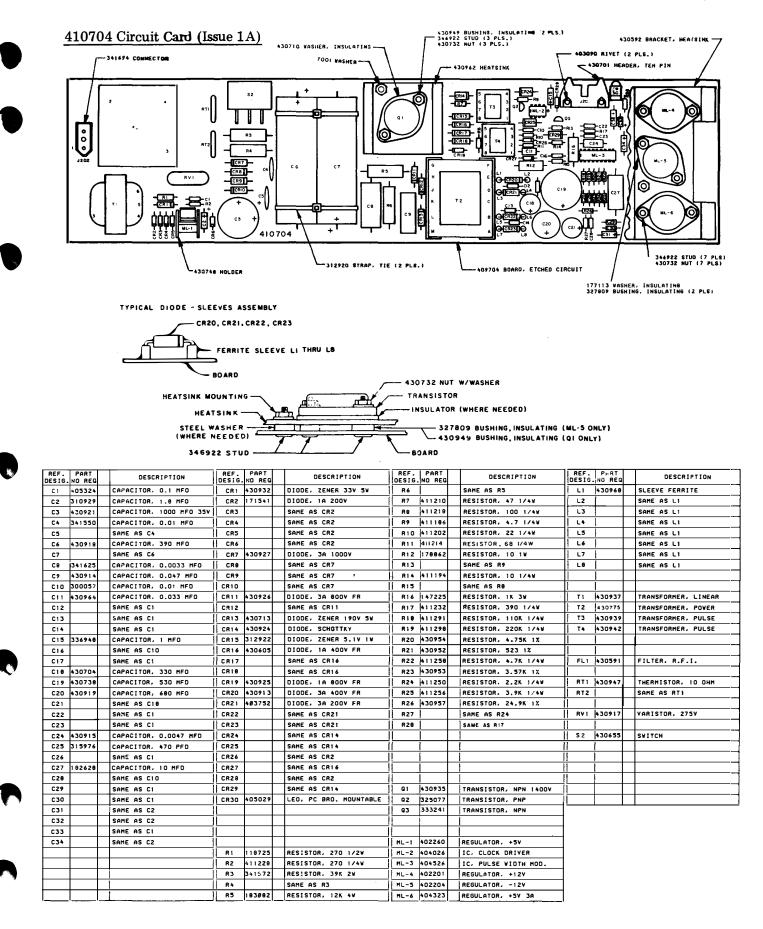


C. 430760 POWER SUPPLY ASSEMBLY (Contd)



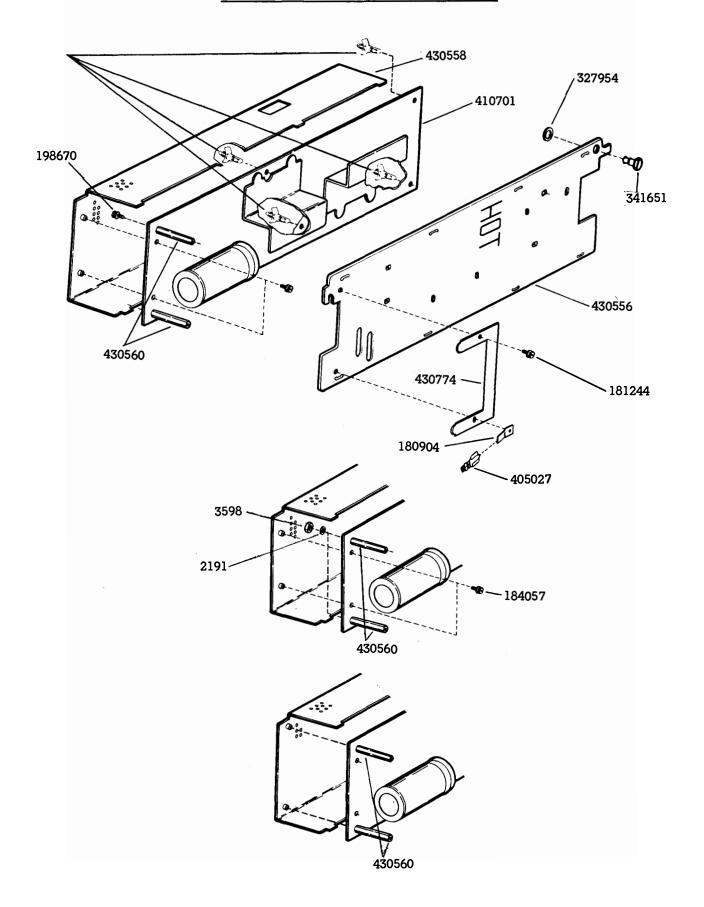
410703 Circuit Card (Issue 1A)

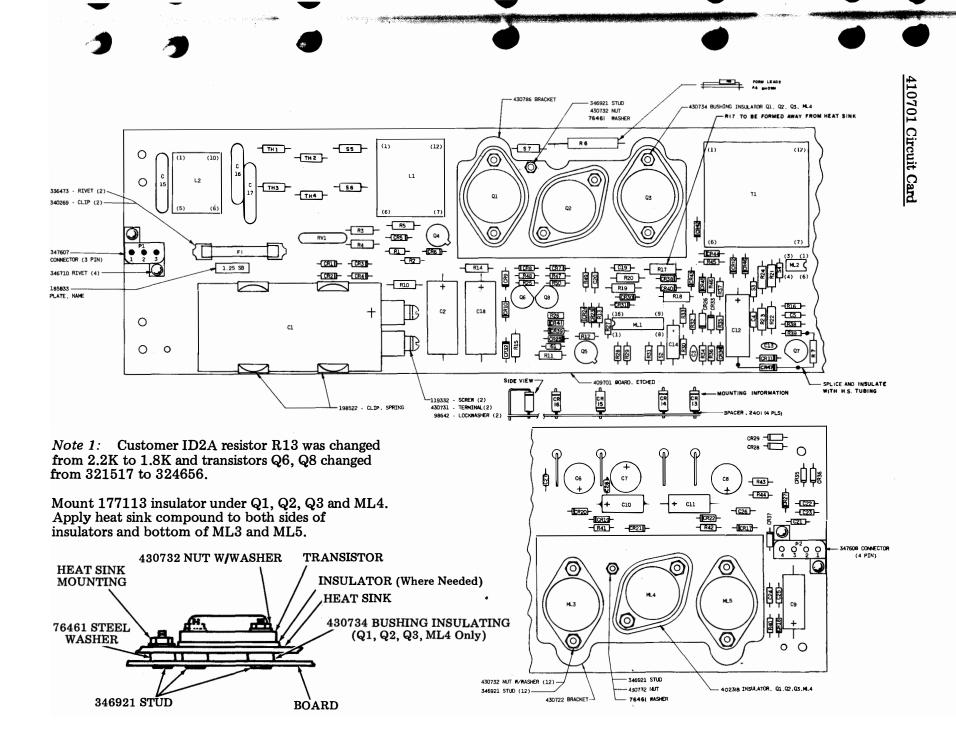
C11 SAME AS C2 CR11 430926 DIODE, 3A BOOV FR R20 SAME AS R9 C12 SAME AS C2 CR12 430713 DIODE, ZENER 190V 5W R21 430957 RESISTOR, 24.9K 1% RESISTOR, 3.57K 1% C13 SAME AS CZ CR13 SAME AS CR11 R22 430953 C14 430919 CAPACITOR, 680 MFO CR14 430913 DIODE, 3A 400V FR RESISTOR, 2.2K 1/4W R23 411250 SAME AS C2 CR15 403752 DIODE, 3A 200V FR RESISTOR, 390 1/4W C15 R24 411232 C16 430736 CAPACITOR, 530 HFD CR16 SAME AS CR15 R25 SAME AS R23 CAPACITOR, 330 MFO R28 411258 RESISTOR, 4.7K 1/4W C17 430704 CR17 SAME AS CR15 C18 SAME AS C17 CR18 430925 DIODE, 1A 900V FR RESISTOR, 3.9K IW R27 178864 C19 300057 CAPACITOR, 0.01 MFO CR19 430605 DICDE, 1A 400V FR 92 430935 TRANSISTOR, NPN 1400V CR20 312922 DIODE, ZENER 5.1V 1W C21 SAME AS C2 REGULATOR: +5V CR21 430924 DIODE, SCHOTTKY HL1 402260 CAP. 470 PFD C22 315976 CR22 SAME AS CR1 HL2 404026 IC. CLOCK DRIVER C23 SAME AS C2 CR23 SAME AS CR19 HL3 404526 IC, PULSE WIDTH MOD. CAPACITOR, 10 MFD REGULATOR: +5V 3A C24 182628 CR24 SAME AS CR19 ML5 404323 C25 SAME AS C19 CR25 SAME AS CR21 REGULATOR, -12V ML6 402204 C26 336949 CAPACITOR, 1 MFO CR26 SAME AS CR1 HL7 402201 REGULATOR, +12V C27 430915 CAPACITOR, 0.0047 MFO CR 35 SAME AS CRI C28 430964 CAPACITOR, 0.033 MFO CR31 405029 FUSE, 1A FAST BLOW LED, PC BOARD MOUNTABLE F1 120139 C29 SAME AS C2 118725 C 30 SAME AS CIS R1 RESISTOR, 270 1/2 W TI 430937 TRANSFORMER, LINEAR C33 SAME AS C2 R2 411228 RESISTOR, 270 1/4W 430938 TRANSFORMER, POWER T2 C34 SAME AS C2 R3 341572 RESISTOR, 39K 2W Т3 430939 TRANSFORMER, PULSE C35 SAME AS C2 R4 SAME AS R3 TA 430942 TRANSFORMER, PULSE R5 RESISTOR, 12K 4W C36 SAME AS C3 183082 FL1 43059 FILTER, R.F.I. C37 SAME AS C3 SAME AS R5 THERMISTOR, 10 OHM R6 RT1 430947 C38 SAME AS C3 SAME AS RTI RT2 RESISTOR, 47 1/4W R9 411210 RV1 430917 VARISTOR, 275V 411218 RESISTOR, 100 1/4W R9 ST2 336470 STRAP . WIRE ST3 SAME AS STA



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D. 430770 POWER SUPPLY ASSEMBLY

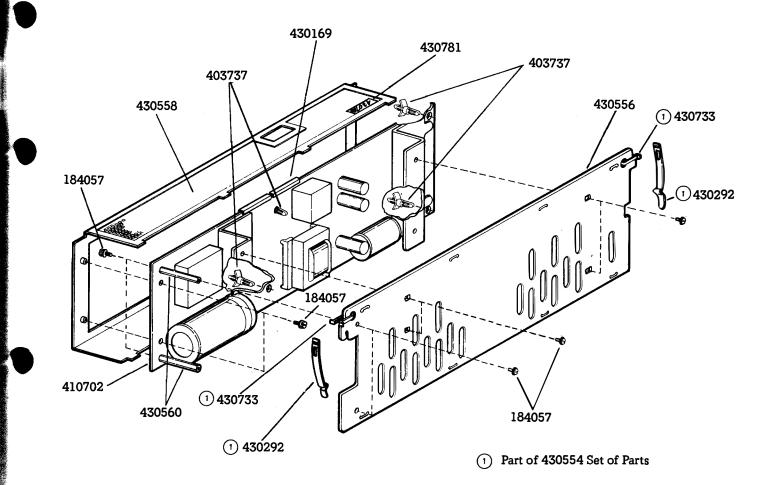




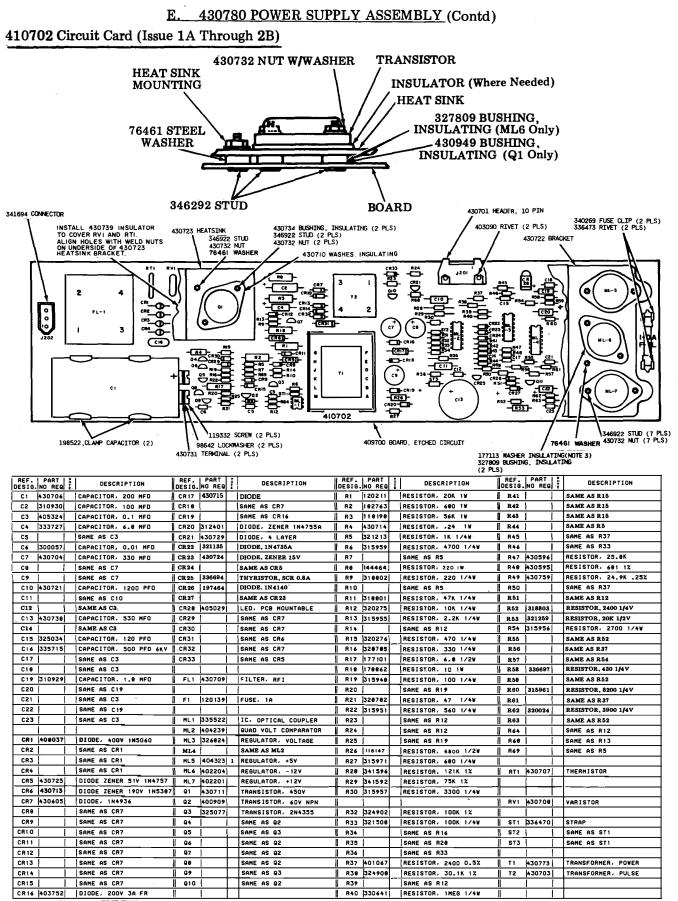
D. 430770 POWER SUPPLY ASSEMBLY (Contd)

	PART	N		0.055		N		REF.	PART	N	, <u> </u>
REF. DESIG,	NO. REQ.	NOTE	DESCRIPTION	DESIG.	PART NO.REQ.	T E	DESCRIPTION	DESIG.	NO. REQ	Ŭ T	DESCRIPTION
C1	430706		CAPACITOR, 200 MFD	R15	311044		RESISTOR .1 3W		198522		CLIP, SPRING
C2	341601		CAPACITOR. 10 MFD	R16	321508		RESISTOR 100K 1/4W	J	430731		TERMINAL CAPACITOR
<u>C3</u>	300057		CAPACITOR, 01 MFD	R17	171580		RESISTOR 470 1W	₩	336473		RIVET
C4 C5	405324		CAPACITOR, 1 MFD	R18	1177600		SAME AS R17	<u> </u>	346710		
C6	430704		SAME AS C4 CAPACITOR, 330 MFD	R19	137602		RESISTOR 47C 1/2W	┨─────	346921		STUD
C7	430704			R20	137601		SAME AS R19 RESISTOR 68: 1/2W	<u>H</u>	76461		WASHER INSULATOR
C8			SAME AS C6 SAME AS C6	R22-24	137001		SAME AS R21		402318		BUSHING, INSULATOR
	182747		CAPACITOR, 60 MFD	R25			SAME AS R2		430732		NUT W/LOCKWASHER
C10	148837		CAPACITOR, 25 MFD		315956		RESISTOR 2.7K 1/4 W		340269		CLIP FUSE
C11			SAME AS C10	R27	324901		RESISTOR 5,49K 1/8W	1	119332		SCREW, ROUND HEAD
C12	192711		CAPACITOR 50 MFD	R28-29			SAME AS R27	<u>ii</u>	98642	Ì	WASHER, LOCK
C13	328793		CAPACITOR .001 MFD	R30	324909		RESISTOR 49.9K 1/4W	1	430722		BRACKET
C14	343698		CAPACITOR .015 MFD	R31	315955		RESISTOR 2.2K 1/4W		430786		BRACKET W/STUDS
C15	405043		CAPACITOR.01 HFD	R32	320275		RESISTOR 10K 1/4W		2401		STUD
C16			SAME AS C15	R33-34	· ·		SAME AS R16	1			
C17			SAME AS C15	R35	318801		RESISTOR 47K 1/4W				
C18			SAME AS C2	R36	315959		RESISTOR 4.7K 1/4W				
C19	430792		CAPACITOR, .0033 MFD	R37-38			SAME AS R32		409701		BOARD, ETCHED
C20			SAME AS CI9	R39			SAME AS R31		185833		PLATE, NAME
C21			SAME AS C4	R40	1		SAME AS R7	1	<u> </u>		1
C22 C23			SAME AS C4 SAME AS C4	R41-42	315948		SAME AS R31 RESISTOR 100 1/4W	<u> </u> 	1	 	1
C24			SAME AS C4	R43	313940		SAME AS R43		1		
C25 1			SAME AS C4	R45-46	s	-	SAME AS R32	<u> </u> тна	430707	I	THERMISTOR 2.50, COLD
C26			SAME AS C4	R45-46			SAME AS R32	1 TH2			SAME AS THI
C27			SAME AS C4	R49			SAME AS R26	<u>і пі</u>	i		SAME AS THI
C28			SAME AS C4	R50			SAME AS R2	1 TH4	i		SAME AS THI
	i			1	i			11	i	i	· ·- ·
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				1							
					430771		TRANSISTOR 500V NPN	1	1		
CR1	312341		DIODE, 1N4004	Q2-Q3	1		SAME AS Q1				
CR2-4 1	1		SAME AS CR1	li Q4	430782		TRANSISTOR 2N 5416	1	1	<u> </u>	1
CR5	430605		DIODE, 1N4936	05	430783	-	TRANSISTOR 2N 3439	-4	 		
CP6-8			SAME AS CR5	Q6	324656	1	TRANSISTOR 2N 3569	<u> .</u>	<u> </u>		
CR9-10			SAME AS CR1		315931		TRANSISTOR 2N 3638		1		
	197464		DIODE, 1N4148	Q8		1	SAME AS Q6	11	<u> </u>		
CR12	470715	ŀ	SAME AS CR11						1	1	
	430715	1	DIODE, 200V 3A	 	1			1	<u> </u>		1
CR14-16 CR17-22		1	SAME AS CR13 SAME AS CR1	<u>n</u>	1	1	1	1	1	1	1
CR23-31	-		SAME AS CR11	<u> </u> F1	307218		FUSE 1.25A SL BL	1	1		· · · ·
	323606	<u>r</u>	DIODE ZENER 20V	1 1	1		, TOL 1.204 3C DL	1	1	1	
	177404		DIODE, ZENER 15V	Î			<u>.</u>	ii	1	i]
CR34	1	-	SAME AS CR33		1			1	1		1
CR35	321161	-	DIODE, ZENER 3.9V	Ï	1			Î.	İ	i	1
	302844		QIODE, ZENER 13V		430784	1	INDUCTOR 4MH	11	İ	İ	1
CR37			SAME AS CR36		430791		INDUCTOR 1MH	1	1	1	
CR38	<u>ا</u>		SAME AS CR5	n			1	ï	1		1
CR39		1	SAME AS CR5	ii ii				ll	1		I
R40-46	I		SAME AS CR11	H	1		l	ÎI.			
CR47	328696		DIODE, ZENER 30V, 1W		1				1		
		1			430772		TRANSFORMER 20 KHZ				
	<u> </u>			1			<u> </u>	11		1	I
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	1	<u> </u>		P1	347607		CONN. PRINTED CKT	<u> </u>	<u> </u>	-	1
ML1	404524 335522	-	PULSE WIDTH MODULATOR	P2	347608		CONN. PRINTED CKT	1	<u> </u> 	-	1
M 0			ISOLATOR, OPTICAL REGULATOR, 12V	<u>1</u>	1	1	1		1	-	1
ML2					I	-	<u>l</u>		<u> </u>	-	1
ML3	402201	-	REGILATOR 12V		1	_	r	<u> </u>	<u>;</u>	-	1
ML3 ML4	402201	-	REGULATOR, 12V		1			0		<u> </u>	•
ML3 ML4	402201	-	REGULATOR, 12V REGULATOR, 5V 3A 	1	430708		VARTSTOR	11			Ī
ML3 ML4	402201	-		1	 430708	<u> </u> {	VARISTOR	<u> </u> 	1	-	1
ML3 ML4	402201	-		1	 430708	 	VARISTOR	<u>∥</u> ╢────	<u> </u>		
ML3 ML4	402201	-		1	 430708 	 	VARISTOR	∥ ┨───	 		
ML3 ML4	402201	-		1	 430708 						
ML3 ML4 ML5	402201		REGULATOR, 5V 3A	 RV1 	 430708 		VARISTOR	Ì			
ML3 ML4 ML5	402201 402204 404323			 RV1 							
ML3 ML4 ML5 R1 R2	402201 402204 404323 1 1 1 1 1 328782		REGULATOR. 5V 3A	RV1			STRAP, ELECTRICAL				
ML3 ML4 ML5 R1 R2	402201 402204 404323 		REGULATOR 5V 3A	RV1			STRAP, ELECTRICAL				
ML3 ML4 ML5 R1 R2 R3	402201 402204 404323 1 1 1 328782 320276 182547		REGULATOR 5V 3A	RV1			STRAP, ELECTRICAL				
ML3 ML4 ML5 R1 R2 R3 R4-5 R6	402201 402204 404323 		REGULATOR, 5V 3A	RV1			STRAP, ELECTRICAL				
ML3 ML4 ML5 R1 R2 R3 R4-5 R6 R7,9	402201 402204 404323 1 328782 320276 182547 161873		REGULATOR 5V 3A	RV1			STRAP, ELECTRICAL				
ML3 ML4 ML5 R1 R2 R3 R4-5 R6 R7,9	402201 402204 404323 1 328782 320276 182547 182547 161873 321213		REGULATOR. 5V 3A RESISTUR. 47 1/4W RESISTUR. 47 1/4W RESISTOR, 470 1/4W RESISTOR, 2.7 1/2W SAME AS R3 RESISTOR. 5K. 5W RESISTOR. 1K 1/4W	RV1			STRAP, ELECTRICAL				
ML3 ML4 ML5 R1 R2 R3 R4-5 R6 R7,9 R10	402201 402204 404323 1 328782 320276 182547 182547 161873 321213		REGULATOR. 5V 3A RESISTOR. 47 1/4W RESISTOR. 47 1/4W RESISTOR. 470 1/4W RESISTOR. 2.7 1/2W SAME AS R3 RESISTOR. 1K 1/4W RESISTOR. 1K 1/4W RESISTOR. 3.9K 1/2W	RV1			STRAP, ELECTRICAL				

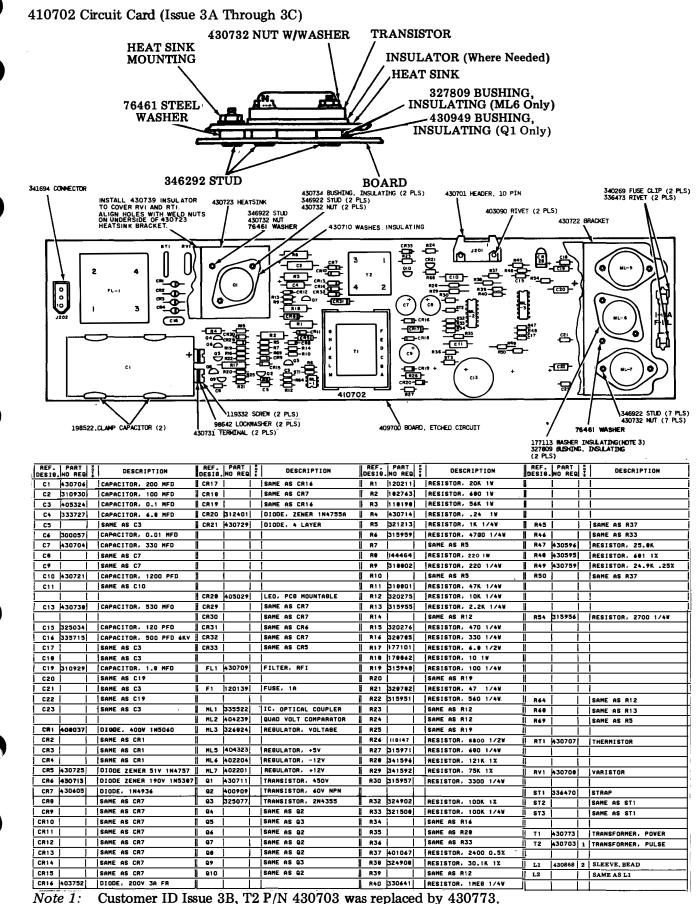
E. 430780 POWER SUPPLY ASSEMBLY



523,	5-1	.4
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Note 1: At customer identification Issue 2A, ML5 was changed from 402202.



Note 1. Customer ID Issue 3D, 121/14 430703 was replaced by

Note 2: Customer ID Issue 3C, L1 and L2 added.

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2401	Stud 12	192711	Capacitor, 50 MFD 12	321259	Resistor, 15 Ohm 5,14
3598	Nut, 6-40 Hex 2,7,10	197464	Diode 3,5,12,14	321507	Resistor, 18,000 Ohm 12
7001	Washer, Flat 8	198522	Clip, Spring 3,5,6,11,12,	321508	Resistor, 100,000 Ohm 4,5,
76461	Washer, Flat 3,5,6,8,11,		14,15		6,12,14,15
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92260	Lockwasher 7		6-40 x 5/16 Hex 10	321786	Plate, Fuse 3
98642	Lockwasher 3,5,6,11,	300057	Capacitor, .01 MFD 3,5,	323606	Diode 12
	12,14,15		6,8,9,12,14,15	324656	Transistor 11,12
118147	Resistor, 6800 Ohm 14,15	300102	Diode 3	324901	Resistor, 5.49K Ohm 12
118157	Resistor, 68K Ohm 12	302844	Diode 12	324902	Resistor, 100,000 Ohm 4,5,
118186	Resistor, 5600 Ohm 4,5,6	307218	Fuse, SL-BL 1-1/4 Amp 12		6,14,15
118198	Resistor, 5600 Ohm 4,5, 6,14,15	310929	Capacitor, 1.8 MFD 3,5,6, 8,9,14,15	324908	Resistor, 30,000 Ohm 4,5, 6,14,15
118725	Resistor, 270 Ohm 8,9	310930	Capacitor, 100 MFD 3,5,6,	324909	Resistor, 49.9K Ohm 12
119332	Screw, 10-32 x 1/4 RD 3,		14,15	325034	Capacitor, 120 PFD 3,5,6,
	5,6,11,12,14,15	311044	Resistor 12		14,15
120139	Fuse, 1 Amp 3,5,6,8,14,	312341	Diode 12	325077	Transistor 4,5,6,9,14,15
	15	312401	Diode 3,5,6,14,15	326823	Regulator, Voltage 3,5
120211	Resistor, 20,000 Ohm 4,5,	312918	Strap, Tie 8	326824	Regulator, Voltage 5,6,14,
	6,14,15	312920	Strap, Cable 9		15
121473	Post 7	312922	Diode 8,9	327721	Resistor, 4.7 Meg Ohm 4,5
137601	Resistor, 68 Ohm 12	315931	Transistor 12	327809	Bushing, Insulating 3,4,5,6,
137602	Resistor, 470 Ohm 12	315948	Resistor, 100 Ohm 4,5,6,		8,9,14,15
143667	Resistor, 3900 Ohm 12		12,14,15	327954	Retainer 10
144464	Resistor, 220 Ohm 4,5,6,	315951	Resistor, 569 Ohm 4,5,6,	328696	Diode 4,12
	14,15		14,15	328782	Resistor, 47 Ohm 5,12,14,
147225	Resistor, 1000 Ohm 8,9	315955	Resistor, 2200 Ohm 4,5,		15
148837	Capacitor, 25 MFD 12		6,12,14,15	328785	Resistor, 330 Ohm 4,5,6,
161873	Resistor, 5000 Ohm 12	315956	Resistor, 2700 Ohm 4,5,		14,15
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171580	Resistor, 470 Ohm 12	315957	Resistor, 3300 Ohm 4,5,6,	330641	Resistor, 1 Meg Ohm 4,5,
177101	Resistor, 6.8 Ohm 4,5,6,		14,15		6,14,15
	14,15	315959	Resistor, 4700 Ohm 4,5,6,	333241	Transistor 9
177113	Insulator 3,5,6,8,9,11,14		12,14,15	333727	Capacitor, 6.8 Ohm 3,5,6,
	15	315961	Resistor, 8200 Ohm 4,5,14		14,15
177404	Diode 12	315971	Resistor, 680 Ohm 4,5,6,	335522	Coupler 3,5,6,12,14,15
178862	Resistor, 10 Ohm 4,5,6,		14,15	335622	Resistor, 68 Ohm 5
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178864	Resistor, 3900 Ohm 8	315988	Resistor, 27,000 Ohm 4,5	336470	Strap 4,5,6,8,12,14,15
180904	Tab Terminal 10	318801	Resistor, 4700 Ohm 4,5,6,	336473	Rivet 3,6,8,11,12,14,15
181244	Screw w/Lockwasher,		12,14,15	336694	Rectifier 3,5,14
	6-40 x 7/16 Hex 10	318802	Resistor, 220 Ohm 4,5,6,	336697	Resistor, 430 Ohm 4,5,14
182547	Resistor 12		14,15	336948	Capacitor, 1.0 MFD 8,9
182628	Capacitor, 10 MFD 8,9	318803	Resistor, 2400 Ohm 4,5,14	340269	Clip, Fuse 3,6,8,11,12,14,
182747	Capacitor, 60 MFD 12	320024	Resistor, 3900 Ohm 5,14		15
182763	Resistor 4,5,6,14,15	320026	Resistor, 3900 Ohm 4	341550	Capacitor, 0.01 MFD 8,9
183082	Resistor, 12K Ohm 8,9	320275	Resistor, 10,000 Ohm 4,5,	341572	Resistor, 39K Ohm 8,9
184056	Screw w/Lockwasher,		6,12,14,15	341592	Resistor, 75,000 Ohm 4,5,
104055	6-40 x 1/4 Hex 7	320276	Resistor, 470 Ohm 4,5,6,		6,14,15
184057	Screw w/Lockwasher,	•	12,14,15	341596	Resistor, 121,000 Ohm 4,5,
104650	6-40 x 3/8 Hex 2,7,10,13	321135	Diode 3,5,14		6,14,15
184058	Screw w/Lockwasher,	321161	Diode 12	341601	Capacitor, 10 MFD 12
	6-40 x 7/16 Hex 7	321213	Resistor 4,5,6,12,14,15		

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		9	411256	Resistor, 3.9K 1/4 W 8,9	430759	Resistor, 24.9K .25% 5,6,
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	341694	Connector 3,5,6,8,9,14,15	411291	Resistor, 110K 1/4 W 8,9	430760	Power Supply Assembly 1,
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	346292	Stud 14,15	430169	Strip, Insulator 2,13	430770	Power Supply Assembly 1,
	346710 346921	Rivet 11,12 Stud 3,5,6,8,11,12	430292 430554	Clamp 2,7,13 Clip 2,7,13	430771	10 Transistor 12
	346921 346922	Stud 5,6,8,9,14,15	430556	Sink, Heat 2,10,13	430772	Transformer 12
	347607	Connector 11,12	430558	Cover 2,10,13	430773	Transformer, Power 5,14,
	347608	Connector 11,12	430560	Post 2,7,10,13	100770	15
	400909	Transistor 4,5,6,14,15	430590	Cover 7	430774	Plate 10
	401067	Resistor, 24,000 Ohm 4,5,	430591	Filter 8,9	430775	Transformer, Power 9
		6,14,15	430592	Bracket 9	430780	Power Supply Assembly 1,
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		15	430596	Resistor 5,6,14,15	430781	Label 13
	402202	Regulator 3,5,6	430605	Diode 3,5,6,8,9,12,14,15	430782	Transistor, 2N 5416 12
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	402260	Regulator 8,9	430664	Plug, Hole 7	430785	Label 2
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	403752	Diode 3,8,9,14,15 Driver, Clock 8,9	430702	Transformer, Pulse 4,5,6,	430868	Diode, 3A 400V FR 8,9
	404239	Circuit, Integrated 3,5,6,	100700	14,15	430914	Capacitor, 0.047 MFD 8,9
	101207	14,15	430704	Capacitor, 330 MFD 3,5,	430915	Capacitor, 0.007 MFD 8,9
, · ·	404323	Regulator 8,9,12,14,15		6,8,9,12,14,15	430917	Varistor, 275V 8,9
	404325	Isolator 4	430705	Capacitor 5	430918	Capacitor, 390 MFD 8,9
	404524	Circuit, Integrated 12	430706	Capacitor, 200 MFD 3,5,	430919	Capacitor, 680 MFD 8,9
	404526	IC, Pulse Width Modulator		6,12,14,15	430921	Capacitor, 1000 MFD 35V
		8,9	430707	Thermistor 4,5,6,12,14,15		8,9
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	405029	Led 3,5,6,8,9,14,15	430709	Filter 3,5,6,14,15	430925	Diode 8,9
	405043	Capacitor, .01 MFD 12	430710	Washer 3,5,6,8,9,14,15	430926	Diode 8,9
	405324	Capacitor, .1 MFD 3,5,6,	430711 430713	Transistor 4,5,6,14,15	430927	Diode 8,9
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	409700	Card, Circuit 5,6,14,15	430715	Diode 3,5,6,12,14	430935	Transistor 9
	409701	Board, Circuit 11,12	430719	Resistor 4,5	430937	Transformer, Linear 8,9
	409703	Board, Circuit 8	430721	Capacitor, 1200 PFD 3,	430938	Transformer, Power 8
	409704	Board, Circuit 9		5,6,14,15	430939	Transformer, Pulse 8,9
	410700	Card, Power Supply 2,3,	430722	Bracket 3,5,6,11,12,14,15	430942	Transformer, Pulse 8,9
		4,5,6	430723	Sink, Heat 3,5,6,14,15	430947	Thermistor, 10 Ohm 8,9
	410701	Card, Circuit 10,11	430724	Diode 3,5,14	430949	Bushing, Insulating 8,9,14,
	410702	Card, Circuit 13,14,15	430725	Diode 3,5,6,14,15		15
	410703	Card, Circuit 7,8	430729	Diode 3,5,6,14,15	430952	Resistor, 523 Ohm 8,9
	410704	Card, Circuit 7,9 Resistor 9	430731	Terminal 3,5,6,11,12,14,15	430953	Resistor, 3.57K Ohm 8,9
	411186 411194	Resistor, 10 1/4 W 8,9	430732	Nut 3,5,6,8,9,11,12,14,15	430954	Resistor, 4.75K Ohm 8,9
	411194	Resistor, 10 1/4 W 8,9 Resistor, 22 1/4 W 8,9	430733	Clip 2,7,13 Bushing Insulating 7.4.5	430957	Resistor, 24.9K Ohm 8,9
	411202	Resistor, 22 1/4 w 8,9 Resistor, 47 Ohm 8,9	430734	Bushing, Insulating 3,4,5, 6,11,12,14,15	430962	Sink, Heat 8,9
	411210	Resistor 9	430738	Capacitor, 530 MFD 3,5,6,	430963 430964	Bracket, Heat Sink 8
	411218	Resistor, 100 1/4 W 8,9	100700	8,9,14,15	430964	Capacitor, 0.033 MFD 8,9 Sleeve, Ferrite 8,9
	411228	Resistor, 270 1/4 W 8,9	430739	Insulator 5,6,14,15	454134	Bumper 7
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PART 6 – PACKING AND MARKING

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A. GENERAL

This part provides packing information for the 430700, 430760, 430770 and 430780 power supply assemblies.

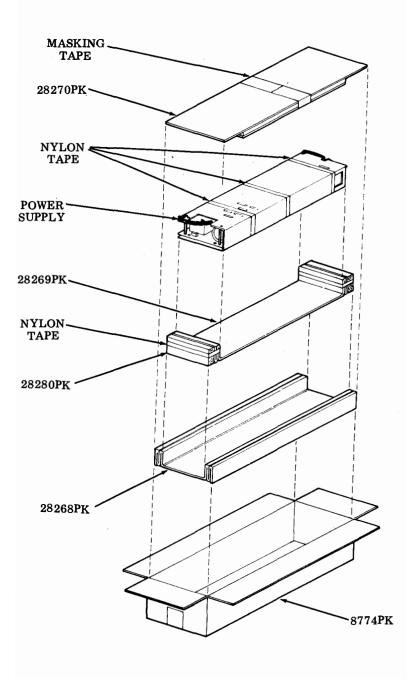
The loose power supply assemblies should be properly packed for storage or transportation between service and customer locations. Packing provides protection against damage or contamination and facilitates storage, stock selection and handling.

The PK packing materials may be obtained from Teletype Corporation.

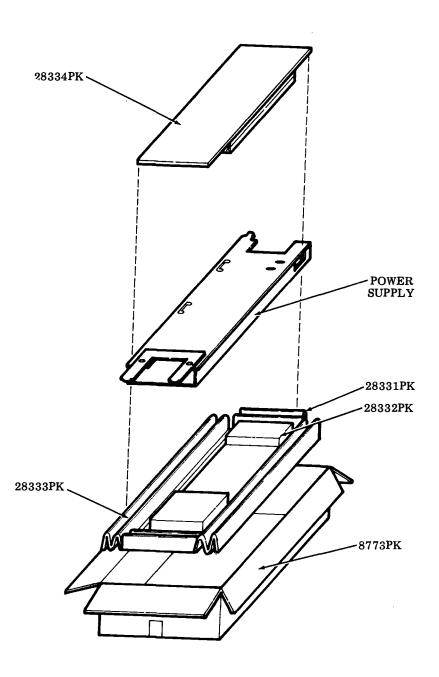
Identify the contents on the outside of each carton after packing, with the code or part number and quantity using idelible markers or premarked adhesive labels.

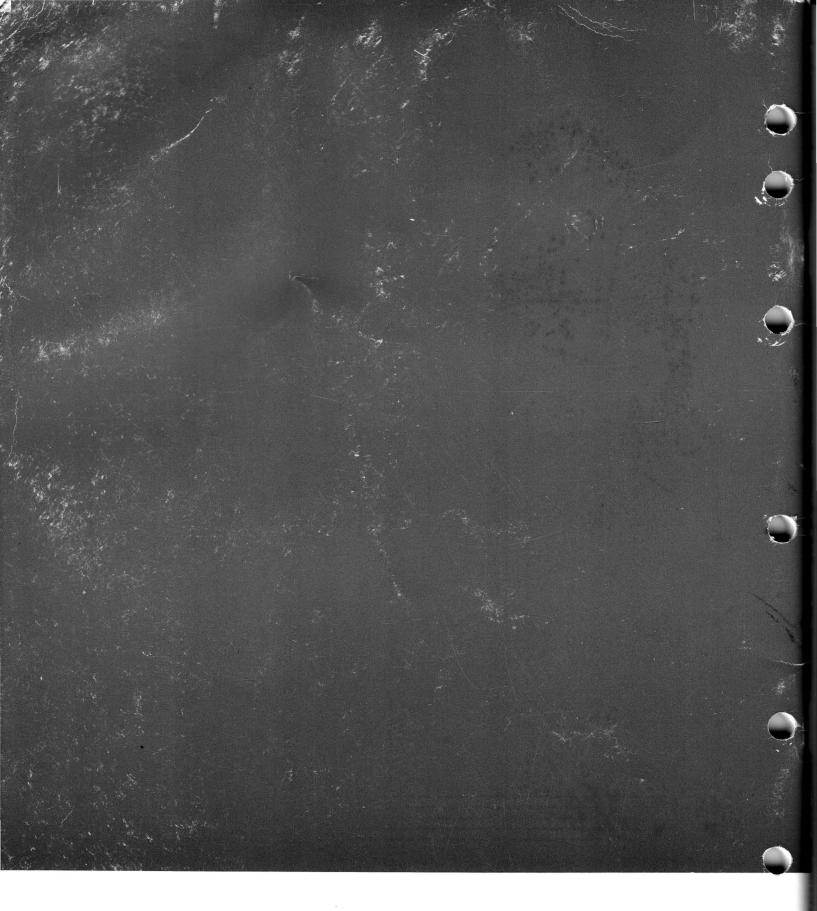
Note: When ordering replaceable parts or components, unless otherwise specified, prefix each part number with the letters "TP" (ie, TP410055).

B. 430700, 430760 AND 430780 POWER SUPPLY PACKING



C. 430770 POWER SUPPLY PACKING







5555 Touhy Avenue Skokie, IL 60077 Phone (312) 982-2000

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